# Tillamook County <br> DEPARTMENT OF COMMUNITY DEVELOPMENT BUILDING, PLANNING \& ON-SITE SANITATION SECTIONS 



## Land of Cheese, Trees and Ocean Breeze

## Floodway Development Permit \#851-21-000321-PLNG: Coulter

> NOTICE TO MORTGAGEE, LIENHOLDER, VENDOR OR SELLER: IRS 215 REQUIRES THAT IF YOU RECEIVE THIS NOTICE, IT MUST BE PROMPTLY FORWARDED TO THE PURCHASER

## NOTICE OF ADMINISTRATIVE REVIEW <br> Date of Notice: March 15, 2022

Notice is hereby given that the Tillamook County Department of Community Development is considering the following:

851-21-000321-PLNG: A review of a Floodway Development Permit for the placement of a proposed single-family dwelling near the Nestucca River. The subject property is accessed from Rueppell Avenue, a County local access road, and is designated as Tax Lot 4800, of Section 30BD of Township 4 South, Range 10 West of the Willamette Meridian, Tillamook County, Oregon. The property is located in the Pacific City/Woods Airpark (PCW-AP) Zone. The applicant is Ronald Coulter. The property owner is David Coulter.

Written comments received by the Department of Community Development prior to 4:00p.m. on March 29, 2022, will be considered in rendering a decision. Comments should address the criteria upon which the Department must base its decision. A decision will be rendered no sooner than the next business day, March 30, 2022.

Notice of the application, a map of the subject area, and the applicable criteria are being mailed to all property owners within 250 feet of the exterior boundaries of the subject parcel for which an application has been made and other appropriate agencies at least 14 days prior to this Department rendering a decision on the request.

A copy of the application, along with a map of the request area and the applicable criteria for review are available for inspection on the Tillamook County Department of Community Development website: https://www.co.tillamook.or.us/commdev/landuseapps and is also available for inspection at the Department of Community Development office located at 1510-B Third Street, Tillamook, Oregon 97141.

If you have any questions about this application, please call the Department of Community Development at 503-842-3408 Ext. 3301 or mjenck@co.tillamook.or.us

Sincerely,


Melissa Jenck, CFM, Land Use Planner II

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## REVIEW CRITERIA

## ARTICLE III - ZONE REGULATIONS

## TCLUO SECTION 3.510: FLOOD HAZARD OVERLAY ZONE

(1) The fill is not within a Coastal High Hazard Area.
(2) Fill placed within the Regulatory Floodway shall not result in any increase in flood levels during the occurrence of the base flood discharge.
(3) The fill is necessary for an approved use on the property.
(4) The fill is the minimum amount necessary to achieve the approved use.
(5) No feasible alternative upland locations exist on the property.
(6) The fill does not impede or alter drainage or the flow of floodwaters.
(7) If the proposal is for a new critical facility, no feasible alternative site is available.
(8) For creation of new, and modification of, Flood Refuge Platforms, the following apply, in addition to (14)(a)(1-4) and (b) (1-5):
i. The fill is not within a floodway, wetland, riparian area or other sensitive area regulated by the Tillamook County Land Use Ordinance.
ii. The property is actively used for livestock and/or farm purposes,
iii. Maximum platform size $=10 \mathrm{sq} \mathrm{ft}$ of platform surface per acre of pasture in use, or 30 sq ft per animal, with a $10-\mathrm{ft}$ wide buffer around the outside of the platform,
iv. Platform surface shall be at least 1 ft above base flood elevation,
v. Slope of fill shall be no steeper than 1.5 horizontal to 1 vertical,
vi. Slope shall be constructed and/or fenced in a manner so as to prevent and avoid erosion.

Conditions of approval may require that if the fill is found to not meet criterion (5), the fill shall be removed or, where reasonable and practical, appropriate mitigation measures shall be required of the property owner. Such measures shall be verified by a certified engineer or hydrologist that the mitigation measures will not result in a net rise in floodwaters and be in coordination with applicable state, federal and local agencies, including the Oregon Department of Fish and Wildlife.


## Vicinity Map



Generated with the GeoMOOSE Printing Utilities

## Zoning Map

## 



Generated with the GeoMOOSE Printing Utilities


# TILLAMOOK County Assessor's Summary Report <br> Real Property Assessment Report 

FOR ASSESSMENT YEAR 2021
March 10, 2022 1:44:05 pm


Comments: $\quad 04-09-04$ Changed land value to reflect residential trends for neighborhood. sm. 10/18/06 input inventory. gb 01/29/14 Reappraised land; tabled values. RBB

## National Flood Hazard Layer FIRMette



## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT


B- $\frac{20.2}{17.5}$ Cross Sections with 1\% Annual Chance 17.5 Water Surface Elevation 8 - - - Coastal Transect
mu ${ }_{513}$ min Base Flood Elevation Line (BFE)
Limit of Study
$=$ Limit of Study
Jurisdiction Boundary
--- --- Coastal Transect Baseline
OTHER FEATURES $\qquad$

MAP PANELS
$\square$

Digital Data Available
No Digital Data Available


O
The pin displayed on the map is an approximate point selected by the user and does not represe an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards
The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on $3 / 10 / 2022$ at 4:42 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.
This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

National Wetlands Inventory
Coulter



March 10, 2022

## Wetlands

Estuarine and Marine Deepwater
Estuarine and Marine Wetland

Freshwater Emergent Wetland
Freshwater Forested/Shrub Wetland
Freshwater Pond

This map is for general reference only. The US Fish and Wildlife Service is not responsible for the accuracy or currentness of the base data shown on this map. All wetlands related data should be used in accordance with the layer metadata found on the Wetlands Mapper web site.

Lake
Other
Riverine



Tillamook County Department of Community Development 1510-B Third Street. Tillamook, OR 97141 | Tel: 503-842-3408 Fax: 503-842-1819 www.co.tillamook.or.us

## PLANNING APPLICATION

Applicant '. (Check Box if Same as Property Owner)
Name: Fonald E.Coulternone: (509) 630.5518
Address: P.O. Box 2323


Email:
Request:

## Addition to Delving

Type II
Type III
Type IV


Clerk's Instrument \#: $\qquad$
Authorization
This permit application does not assure permit approval. The applicant and/or property owner shall be responsible for obtaining any other necessary federal, state, and local permits. The applicant verifies that the information submitted is complete, accurate, and consistent with other information submitted with this application.


Tillamook County Department of Community Development 1510-B Third Street. Tillamook, OR 97141 | Tel: 503-842-3408 Fax: 503-842-1819 www.co.tillamook.or.us

## PLANNING APPLICATION



Email:

## Request: Addition to Dwelning



Clerk's Instrument \#: $\qquad$

## Authorization

This permit application does not assure permit approval. The applicant and/or property owner shall be responsible for obtaining any other necessary federal, state, and local permits. The applicant verifies that the information submitted is complete, accurate, and consistent with other information submitted with this application.


COULTER ARCHITECTURE

# David and Pattie Coulter, Single-family Residence Addition. 35465 Rueppell Ave. Pacific City, Oregon 

## MEMO

Melissa, My mailed in submittal is in two packages and includes the following:
(2) Sets of Architectural and Structural Drawings. See index

Photos of the existing building, so you would not have to visit the site. We are replacing the decks ( in the same configuration) which are falling apart plus redoing the windows, doors and siding, and revising the entrance (eliminating the front stair.

Community Development checklist (I Assume you check the boxes.)

Spec sheet on the special Neopor insulation in case you are not familiar with it.
(2) bound books that include the following:

| 1-Project preamble: | Project description |
| :---: | :---: |
| 2-Energy forms: | Additional Measures Selection form |
| 3-Structural Calculations: | FORTE -Gravity plus Lateral computations. |
| 4-Building Details: | Construction Details |
| 5-Soils Report: | Morgan Civil Engineers |

COULTER ARCHTECTURE

6-Property Surveyor:<br>Bayside Surveying, LLC

7-Project Specifications and catalogue cut sheets

The Hydraulics Analysis Report, dated March 30, 2021 was submitted to you previously, and forwarded to FEMA by you, per your request.

Color perspective renderings to help explain the project.

Utility statements showing connection and services to the property for Power, water and Sewer.


## COULTER ARCHTECTURE



105 N. Emerson Street, Suite 201, Chelan, Washington Mail: P.O. Box 2323, Lake Chelan, WA 98816

Office: 509.630 .5518


COULTER ARCHITECTURE

## David and Pattie Coulter, Single-family Residence Addition.

## 35465 Rueppell Ave. Pacific City, Oregon

Project preamble:

Energy forms:

Structural Calculations:

Building Details:

Soils Report:

Property Surveyor:

Project description

Additional Measures Selection form FORTE -Gravity plus Lateral computations.

Construction Details

Morgan Civil Engineers

Bayside Surveying, LLC

Project Specifications and catalogue cut sheets:


David M. Coulter, Single family residence addition. 35465 Rueppell, Pacific City, Oregon

PROJECT INDEX

## PROJECT PREAMBLE:

## PROJECT DRAWINGS INDEX:

| A-0.1 | Site Plan |
| :--- | :--- |
| A-1.1 | First Floor Plan |
| A-1.2 | Second Floor Plan |
| A-1.3 | Door and Window Schedules and roof Plan |
| A-2.1 | South and East Elevations |
| A-2.2 | North and West Elevations |
| A-3.1 | Sections |
| S-1.1 | Foundation Planning |
| S-1.1a | Foundation Details |
| S-1.2 | Second Floor Framing Plan |
| S-1.3 | Roof Framing and SIP Panel Plan |
| S-1.4 | Shear Wall Plans and Details |
| S-1.5 | Structural Notes |
| E-1.1 | First Floor Electrical Plan |
| E-1.2 | Second Floor Electrical Plan |

## RESIDENTIAL ENERGY ADDITIONAL MEASURES SELECTION:

## PROJECT SPECIFICATIONS:

Including Catalog Cuts

## PROJECT ENCLOSURES:

By reference and previously submitted to Tillamook County Planning, and subsequently submitted to FEMA by Tillamook County:
Waterways Consulting, Inc. Hydraulics Analysis Report, dated March 30, 2021

David M. Coulter, Single family residence addition.
35465 Rueppell, Pacific City, Oregon

## PROJECT PREAMBLE

## Project Description:

This project includes an existing house, constructed approximately 30 years ago, with deferred maintenance, and the addition of a new Master suite in the rear yard, making this a four bedroom house with additional entertainment deck.

## Existing House scope :

The existing house is a two story building with the first story built with Concrete Masonry Unit perimeter walls, containing 5 garage stalls. The second story is a three bedroom area of 1809 S.F. of finished space.
The scope of this phase is to provide new decks, replacing the preexisting in the same configuration and footprint as the existing decks. ( see survey site plan.)
The exterior siding will be replaced with new siding, including any deterioration of the sub structure.
All windows and sliding doors will also be replaced with double glazed vinyl windows.
New aluminum garage doors, and a new front entrance replacing the existing exterior stair as the main entrance.

## New Master Suite Addition scope:

The addition of a Master suite upper floor of 1606 S.f. of finished area and a large outdoor deck, both for entertaining and accommodating a large family. The first floor of the new addition is constructed of concrete up to the $16.6^{\prime}$ MSL elevation, providing a flood resistant first story. The first story consists of a two stall garage and a two stall carport, all configured to comply with the Hydrologists analysis to the flood criteria of FEMA. See the report from Waterways Consulting Inc. dated March 30, 2021

## Design Criteria:

Tillamook land use Ordinance 3.510 ( FH ):
FEMA Flood way Zone AE ( per Jake Hofeld, PE of Waterways Consulting, Inc.)
No scour or erosion is anticipated, and wave action should not be a consideration. ( see attached email from Jake Hofeld, PE, dated April 14, 2021 )

Hydraulics Analysis Report, prepared by Waterways Consultants, Inc, dated March 30, 2021 has been submitted to Tillamook County on April 19, 2021. This report establishes the viability of the finish lower floor set at elevation 13.0' MSL. The elevations are based on the topographic survey by Bayside Survey, Inc., by Dallas W. Esplin, dated October 13, 2020. (enclosed)

Flood level established at $16.6^{\prime}$ MSL per Tillamook County Planning Dept. (Specified NAVD 88)

## 5 - Construction Materials and Methods:

(d) All materials on the ground level are either concrete, or located above the 16.6' MSL level.
(E) The project maximizes the practice of minimizing flood water damage.
(f ) All electrical, HVAC, and plumbing are located above (except for piping), and the elevator and its electronics and controllers are located at the top of the shaft of above 16.6 MSL. The elevator is also programmed to return to the upper floor when not is use.

## 6 - Specific standards for A Zones:

(b) The lower level of the building is not subject to any wave action nor is it anticipated to have any scouring or erosion, per the email from the Hydrologist, listed above. We don't anticipate any flood forces acting on the building.
We comply with (6) (b) (1) and (2), providing the required and appropriate openings as shown on the foundation Plan.

Project designed to the 2018 edition of the IRC and the Oregon designated building codes. Section R322.2 Flood Hazard areas (including A Zones )

R322.2.1 Elevation requirements, exception complying with R322.2.2 Enclosed areas below design flood elevation: This project is designed based on this exception, and the elevation of the first level is a product of the flood modeling done by Waterways Consulting, Inc. ( See the referenced report.) Elevaqtion13.0' MSL is established by this report.

2,1- The lower lever is reserved for parking, building access, and storage.
2.2- Flood openings have been provided, see the foundation plan.

R322.2.3 Foundation design and construction: Hydrostatic forces are not a design factor based on the recommendations by Waterways Consulting, Inc. as per email enclosed.
The foundation design is based on the soils report from Morgan Civil Engineering, Inc., and based on that report, at the time of excavation, we will have Jason Morgan, PE look at the site for a final review and recommendations.

## Section 3.335 (3) (1) of the PCW-AP Zone with the Airport Overlay Zone.

Section 3.565 call for two height zones, 33 ' in zone A and 37 feet in zone B. These are MSL numbers, and not building heights from grade.
Melissa Jenk provided an ariel photo of the airport depicting the boundaries of zones A \& B.
We aligned the GIS maps with this site and determined where these zone lines appeared on our site. These zone lines are depicted on our site plan drawing-----------
We submitted these boundary lines to Tillamook County on January 19, 2021, and received a response on January 20, 2021 approving these boundary lines.

## Soils Considerations for founding:

The soil assessment is prepared by Morgan Civil Engineering, Inc, dated April 29, 2021, and specifies the soil bearing capacity of 1500 pounds per square foot. When this is modified on the drawings, this is also recommended by the engineer, or implemented by the Architect based on his judgment.

Jake Hofeld Wed, Apr 14, 1:08 PM (9 days ago)
to me

Hi Ron,

Given how shallow flooding would be at your property, I don't expect scour/erosion to be an issue.

Regarding the flood zone designation, assume this is a Zone A area (the AE is a subcategory of these zones). Therefore, wave action should not be a consideration.

Hope this helps.

Jake D. Hofeld PE/CWRE
Senior Engineer
Waterways Consulting, Inc.
503-528-4816
www.watways.com


## Residential Energy Additional <br> Measure Selection

Department of Consumer and Business Services
Building Codes Division
1535 Edgewater NW. Salem, Oregon
Mailing address: P.O. Box 14470, Salem, OR 97309-0404
503-378-4133 • Fax: 503-378-2322
Web: oregon.govibcd


## Please select type of construction below; sign, date, and complete the entire form. Submit this form with

 your permit application or your project will be placed on hold until the required information is provided.New construction. All conditioned spaces within residential buildings must comply with Table N1101.1(1) and two additional measures (one numbered and one lettered) from Table N1101.1(2) on Page 2.
Additions. Additions to existing buildings or structures may be made without making the entire building or structure comply if the new additions comply with the requirements of this chapter. (N1101.3)
Large additions. Additions that are equal to or more than 40 percent of the existing building heated floor area or 600 square feet ( $55 \mathrm{~m}^{2}$ ) in area, whichever is less, must comply with Table N1101.1(2) on Page 2. (N1101.3.1) (Note: You must select one numbered and one lettered measure.)Small additions. Additions that are less than 40 percent of the existing building heated floor area or less than 600 square feet ( $55 \mathrm{~m}^{2}$ ) in area, whichever is less, must select one measure from Table N1101.1(2) on page 2 or comply with Table N1101.3 below. (N1101.3.2)
$\square$ Exception: Additions that are less than 15 percent of existing building heated floor area or 200 square feet ( $18.58 \mathrm{~m}^{2}$ ) in area, whichever is less, are not required to comply with Table N1101.1(2) or Table N1101.3.

Selected item number: $\qquad$ Selected item letter:
Note: Depending on which Additional Megsums you have selected, there may be sub-options that you will have to specify. Check the appropriate b

Applicant's signature:


Print name: $\qquad$ Coulter, 6 IA
VAL ME ASURES (SELECT ONE)
TABLE N1101.3 - SMALL ADDITION ADDITIONAL MEASURES (SELECT ONE)

| $\square$ | 1 | Increase the ceiling insulation of the existing portion of the home as specified in Table N1101.2. |
| :---: | :---: | :--- |
| $\square$ | 2 | Replace all existing single-pane wood aluminum windows to the U-factor as specified in Table N1101,2. |
| $\square$ | 3 | Insulate the floor system as specified in Table N1101.2 \& install 100 percent of permanently installed lighting fixtures as <br> CFL, LED, or linear fluorescent or a minimum efficacy of 40 lumens per watt as specified in Section N1107.2. |
| $\square$ | 4 | Test the entire dwelling with a blower door and exhibit no more than 6.0 air changes per hour @ 50 Pascals. |
| $\square$ | 5 | Seal and performance test the duct system. |
| $\square$ | 6 | Replace existing 78 percent AFUE or less gas furnace with a 92 percent AFUE or greater system. |
| $\square$ | 7 | Replace existing electric radiant space heaters with a ductless mini split system with a minimum HSPF of 10.0. |
| $\square$ | 8 | Replace existing electric forced air furnace with an air source hedpump with a minimum HSPF of 9.5. |
| $\square$ | 9 | Replace existing water heater with a water heater meeting Conservation Measure D [Table N1101.1(2)]. |

TABLE N1101.1(2) ADDITIONAL MEASURES

|  | $\square$ | 1 | High-efficiency walls |
| :---: | :---: | :---: | :---: |
|  |  |  | Exterior walls - U-0.045/R-21 cavity insulation $+\mathrm{R}-5$ contimuous |
|  |  | 2 | Upgraded features |
|  |  |  | Exterior walls - U-0.057 / R-23 intermediate or R-21 advanced, Framed floors - U-0.026 / R-38, and Windows - U-0.28 (average UA) |
|  | $\square$ | 3 | Upgraded features |
|  |  |  | Exterior walls - U-0.055 / R-23 intermediate or R-21 advanced, <br> Flat ceiling - U-0.017/R-60, and <br> Framed floors - U-0.026 i R-38 |
|  | $\square$ | 4 | Super Insulated Windows and Attic OR Framed Fioors |
|  |  |  | Windows - U-0.22 (Triple Pane Low-e), and Flat ceiling ${ }^{\text {e }}$ - U-0.017 / R-60 or Framed floors - U-0.026 / R-38 |
|  | $\square$ | 5 | Air sealing bome and ducts |
|  |  |  | Mandatory air sealing of all wall coverings at top plate and air sealing checklist ${ }^{t}$, and Mechanical whole-building ventilation system with rates meeting M1507.3 or ASHRAE 62.2, and All ducts and air handlers contained within building envelope ${ }^{\text {d }}$ or All ducts sealed with mastic ${ }^{\text {b }}$ |
|  | $\square$ | 6 | High efficiency thermal envelope UA ${ }^{\text {B }}$ |
|  |  |  | Proposed UA is $8 \%$ lower than the code UA |
|  |  |  |  |
|  | $\square$ | A | High efficicncy HVAC system ${ }^{\text {a }}$ |
|  |  |  | Gas-fired furnace or boiler AFUE 94 percent, or Air source heat pump HSPF 9.5/15.0 SEER cooling, or Ground source heat pump COP 3.5 or Energy Star rated |
|  | $\square$ | $B$ | Ducted HVAC systems within conditioned space |
|  |  |  | All ducts and air handlers contained within building envelope ${ }^{d}$ Cannot be combined with Measure 5 |
|  |  | C | Ductless heat pump |
|  |  |  | Ductless heat pump HSPF 10.0 in primary zone of dwelling |
|  | $x$ | D | High efficiency water heater ${ }^{\text {c }}$ |
|  |  |  | Natural gas/propane water heater with UEF 0.85 or <br> Electric heat pump water heater Tier 1 Northern Climate Specification Product |

For SI: I square foot $=0.093 \mathrm{~m}^{2}, 1$ watt per square foot $=10.8 \mathrm{~W} \mathrm{~m}^{2}$.
a. Appliances located within the buiding thermal envelope shall have sealed combustion air installed. Combustion air shall be ducted directly from the outdoors.
b. All duct joints and seams sealed with listed mastic; tape is allowed only at appliance or equipment connections (for service and replacement). Meet sealing criteria of Performance Tested Comfort Systems program administered by the Bonneville Power Administration (BPA).
c. Residential water heaters less than 55 -gallon storage volume.
d. A total of 5 percant of an HVAC system's ductwork shall be permitted to be located outside of the conditioned space. Ducts located outside the conditioned space shall have insulation installed as required in this code.
e. The maximum vaulted ceiling surface area shall not be greater than 50 percent of the total heated space floor area uriess vatited area has a U-factor no greater than U-0.026.
f. Continuous air barrier. Additional requircment for saling of all interior vertical wall covering to top plate framing. Sealing with foam gasket, caulk, or other approved sealant listed for sealing wall covering material to structumal material (example: gypsum board to wood stad framing).
g. Table NIIO4.1(1) Standard base case design, Code UA shall be at least 8 percent less than the Proposed UA. Buildings with fenestration less than 15 percent of the total vertical wall area, these buildings may adjust the Code UA to have 15 percent of the wall area as fenestration.

| Level |  |  |  |
| :---: | :---: | :---: | :---: |
| Member Name | Results | Current Solution | Comments |
| Carport Beam B1 | Passed | 1 piece(s) $51 / 8^{\prime \prime} \times 131 / 2^{\prime \prime} 24 F-V 4$ DF Glulam |  |
| Floor: Flush Beam B2 | Passed | 2 piece(s) $13 / 4^{\prime \prime} \times 91 / 4^{\prime \prime} 2.0$ E Microllam® LVL |  |
| Garage Beam B3 | Passed | 1 piece(s) $51 / 8^{\prime \prime} \times 131 / 2^{\prime \prime} 24 F-V 4$ DF Glulam |  |
| Garage Beam B4 | Passed | 1 piece(s) $51 / 8^{\prime \prime} \times 131 / 2^{\prime \prime} 24 F-V 4$ DF Glulam |  |
| Deck Beam B5 | Passed | 1 piece(s) $31 / 8^{\prime \prime} \times 18^{\prime \prime} 24 \mathrm{~F}-\mathrm{V} 4$ DF Glulam |  |
| Deck Beam B6 | Passed | 1 piece(s) $51 / 8^{\prime \prime} \times 131 / 2^{\prime \prime} 24 F-V 4$ DF Glulam |  |
| Deck Beam B7 | Passed | 1 piece(s) $31 / 8^{\prime \prime} \times 131 / 2^{\prime \prime} 24 F-V 4$ DF Glulam |  |
| Deck Beam B8 | Passed | 1 piece(s) $31 / 8^{\prime \prime} \times 131 / 2^{\prime \prime} 24 F-V 4$ DF Glulam |  |
| Garage Beam B9 | Passed | 2 piece(s) $13 / 4^{\prime \prime} \times 91 / 4^{\prime \prime} 2.0$ E Microllam® LVL |  |
| Garage Door Header H-6 | Passed | 2 piece(s) $13 / 4^{\prime \prime} \times 91 / 4^{\prime \prime} 2.0$ E Microllam® LVL |  |
| Deck Beam B11 | Passed | 2 piece(s) $13 / 4^{\prime \prime} \times 91 / 2^{\prime \prime} 2.0$ E Microllam® LVL |  |
| Deck Beam B17 | Passed | 1 piece(s) $31 / 8^{\prime \prime} \times 18^{\prime \prime} 24 \mathrm{~F}-\mathrm{V} 4$ DF Glulam |  |
| Deck Beam B18 | Passed | 1 piece(s) $31 / 8^{\prime \prime} \times 18^{\prime \prime} 24 \mathrm{~F}-\mathrm{V} 4$ DF Glulam |  |
| Roof |  |  |  |
| Member Name | Results | Current Solution | Comments |
| Roof Beam B-10 | Passed | 1 piece(s) $51 / 8^{\prime \prime} \times 18{ }^{\prime \prime} 24 F-$ V8 DF Glulam |  |
| H-1 | Passed | 2 piece(s) $13 / 4^{\prime \prime} \times 111 / 4^{\prime \prime} 2.0 \mathrm{E}$ Microllam® LVL |  |
| H-2 | Passed | 2 piece(s) $13 / 4^{\prime \prime} \times 111 / 4^{\prime \prime} 2.0$ E Microllam® LVL |  |
| H-3 | Passed | 2 piece(s) $2 \times 10$ DF No. 1 |  |
| H-4 | Passed | 2 piece(s) $2 \times 8$ DF No. 1 |  |
| H-5 | Passed | 2 piece(s) $2 \times 8$ DF No. 1 |  |
| H-6 | Passed | 2 piece(s) $13 / 4^{\prime \prime} \times 91 / 2^{\prime \prime} 2.0$ E Microllam® LVL |  |
| Existing House |  |  |  |
| Member Name | Results | Current Solution | Comments |
| Deck Beam B12 | Passed | 1 piece(s) $31 / 8^{\prime \prime} \times 18^{\prime \prime} 24 \mathrm{~F}-\mathrm{V} 8$ DF Glulam |  |
| Ridge Beam B13 | Passed | 1 piece(s) $51 / 8^{\prime \prime} \times 101 / 2^{\prime \prime} 24 F-V 8$ DF Glulam |  |
| Gable Beam B14 | Passed | 1 piece(s) $51 / 8^{\prime \prime} \times 161 / 2^{\prime \prime} 24 F-V 4$ DF Glulam |  |
| Deck Beam B15 | Passed | 2 piece(s) $13 / 4^{\prime \prime} \times 18^{\prime \prime} 2.0 \mathrm{E}$ Microllam® LVL |  |
| Deck Beam B16 | Passed | 1 piece(s) $51 / 8^{\prime \prime} \times 18^{\prime \prime} 24 \mathrm{~F}-\mathrm{V} 8$ DF Glulam |  |


| ForteWEB Software Operator | Job Notes |
| :--- | :--- |
| Ron Coulter |  |
| Coulter Architects PLLC |  |
| (509) $630-5518$ <br> rkent.architecture@gmail.com |  |



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | 18506 @ $12^{\prime} 6^{\prime \prime}$ | $18322\left(5.50^{\prime \prime}\right)$ | Passed (101\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (Ibs) | $7605 @ 13^{\prime} 101 / 4^{\prime \prime}$ | 12223 | Passed (62\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Pos Moment (Ft-lbs) | 15286 @ $19^{\prime} 77 / 8^{\prime \prime}$ | 31134 | Passed (49\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (Alt Spans) |
| Neg Moment (Ft-lbs) | $-22515 @ 12^{\prime} 6^{\prime \prime}$ | 23999 | Passed (94\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.132 @ 6^{\prime} 13 / 16^{\prime \prime}$ | 0.304 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0$ L (Alt Spans) |
| Total Load Defl. (in) | $0.185 @ 5^{\prime} 103 / 4^{\prime \prime}$ | 0.608 | Passed (L/788) | -- | $1.0 \mathrm{D}+1.0$ L (Alt Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length $L=10^{\prime} 5 / 16^{\prime \prime}$.
- Critical negative moment adjusted by a volume factor of 1.00 that was calculated using length $L=6^{\prime} 1^{\prime \prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1 - Column - DF | 5.50" | 4.25" | $1.91{ }^{\prime \prime}$ | 2431 | 4073/-473 | $\begin{gathered} 6504 /- \\ 473 \end{gathered}$ | 1 1/4" Rim Board |
| 2 - Column - DF | 5.50 " | 5.50 " | 5.56" | 7556 | 10950 | 18506 | None |
| 3 - Column - DF | 5.50" | 4.25" | 1.91" | 2431 | 4073/-473 | $\begin{gathered} 6504 /- \\ 473 \end{gathered}$ | 1 1/4" Rim Board |

- Rim Board is assumed to carry all loads applied directly above it, bypassing the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $24^{\prime} 10^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $24^{\prime} 10^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

|  |  |  | Dead | Floor Live |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Vertical Loads | Location (Side) | Tributary Width | $\mathbf{( 0 . 9 0 )}$ | $\mathbf{( 1 . 0 0 )}$ | Comments |
| 0 - Self Weight (PLF) | $11 / 4^{\prime \prime}$ to $24^{\prime} 103 / 4^{\prime \prime}$ | N/A | 16.8 | -- |  |
| 1 - Uniform (PSF) | 0 to $25^{\prime}$ (Front) | $12^{\prime}$ | 40.0 | 60.0 | Default Load |

## Weyerhaeuser Notes




 and/or tested in accordance with applicable ASTM standards. For current code evaluation reports, Weyerhaeuser product literature and installation details refer to www.weyerhaeuser.com/woodproducts/document-library.
The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

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Level, Floor: Flush Beam B2
2 piece(s) 1 3/4" x 9 1/4" 2.0E Microllam® LVL


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | 2538 @ $4^{\prime \prime}$ | $9297\left(4.25^{\prime \prime}\right)$ | Passed (27\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $2089 @ 1^{\prime} 23 / 4^{\prime \prime}$ | 6151 | Passed (34\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | 7493 @ $6^{\prime} 51 / 2^{\prime \prime}$ | 11204 | Passed (67\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.303 @ 6^{\prime} 51 / 2^{\prime \prime}$ | 0.306 | Passed (L/486) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | $0.465 @ 6^{\prime} 51 / 2^{\prime \prime}$ | 0.613 | Passed (L/316) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor Member Type : Flush Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - DF | 5.50" | 4.25" | 1.50" | 900 | 1679 | 2579 | $11 / 4^{\prime \prime}$ Rim Board |
| 2 - Stud wall - DF | $5.50{ }^{\text {" }}$ | 4.25" | 1.50 " | 900 | 1679 | 2579 | 11/4" Rim Board |

- Rim Board is assumed to carry all loads applied directly above it, bypassing the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $12^{\prime} 9^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $12^{\prime \prime} 9^{\prime \prime} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

|  |  |  | Dead | Floor Live |  |
| :--- | :---: | :---: | :---: | :---: | :--- |
| Vertical Loads | Location (Side) | Tributary Width | $\mathbf{( 0 . 9 0 )}$ | $\mathbf{( 1 . 0 0 )}$ | Comments |
| 0 - Self Weight (PLF) | $11 / 4^{\prime \prime}$ to $12^{\prime} 93 / 4^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 9.4 | -- |  |
| 1 - Uniform (PSF) | 0 to $12^{\prime} 11^{\prime \prime}$ (Front) | $6^{\prime} 6^{\prime \prime}$ | 20.0 | 40.0 | Default Load |

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|  |  |



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | 6268 @ 2" | $11211\left(3.50^{\prime \prime}\right)$ | Passed (56\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (Ibs) | 4992 @ $1^{\prime} 5^{\prime \prime}$ | 12223 | Passed (41\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Pos Moment (Ft-lbs) | 20776 @ $6^{\prime} 111 / 2^{\prime \prime}$ | 31134 | Passed (67\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Live Load Defl. (in) | 0.275 @ $6^{\prime} 111 / 2^{\prime \prime}$ | 0.453 | Passed (L/592) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Total Load Defl. (in) | $0.365 @ 6^{\prime} 111 / 2^{\prime \prime}$ | 0.679 | Passed (L/447) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |

System : Floor
Member Type : Drop Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length $\mathrm{L}=13^{\prime} 7^{\prime \prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  |  | Loads to Supports (Ibs) |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Stud wall - DF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.96^{\prime \prime}$ | 1537 | 4732 | 6269 | Blocking |
| 2 - Stud wall - DF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.96^{\prime \prime}$ | 1537 | 4732 | 6269 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $13^{\prime} 11^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $13^{\prime} 11^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $\mathbf{( 1 . 0 0 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $13^{\prime} 11^{\prime \prime}$ | N/A | 16.8 | -- |  |
| 1 - Uniform (PSF) | 0 to $13^{\prime} 11^{\prime \prime}$ (Front) | $17^{\prime}$ | 12.0 | 40.0 | Default Load |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (Ibs) | 10589 @ $15^{\prime} 81 / 4^{\prime \prime}$ | $11211\left(3.50^{\prime \prime}\right)$ | Passed (94\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | 6668 @ $14^{\prime} 5^{\prime \prime}$ | 12223 | Passed (55\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Pos Moment (Ft-lbs) | 25406 @ $7^{\prime} 81 / 8^{\prime \prime}$ | 31134 | Passed (82\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (Alt Spans) |
| Neg Moment (Ft-lbs) | $-12765 @ 15^{\prime} 81 / 4^{\prime \prime}$ | 23999 | Passed (53\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Live Load Defl. (in) | $0.469 @ 7^{\prime} 111 / 8^{\prime \prime}$ | 0.517 | Passed (L/397) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (Alt Spans) |
| Total Load Defl. (in) | $0.574 @ 7^{\prime} 101 / 16^{\prime \prime}$ | 0.776 | Passed (L/325) | -- | $1.0 \mathrm{D}+1.0$ L (Alt Spans) |

System : Floor Member Type : Drop Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Overhang deflection criteria: $\operatorname{LL}(2 L / 360)$ and $T L(2 L / 240)$. Upward deflection on right cantilever exceeds overhang deflection criteria.
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length $L=15^{\prime} 1 / 4^{\prime \prime}$.
- Critical negative moment adjusted by a volume factor of 1.00 that was calculated using length $L=6^{\prime} 1111 / 16^{\prime \prime}$.
- Upward deflection on right cantilever exceeds $0.4^{\prime \prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

|  | Bearing Length |  |  |  | Loads to Supports (Ibs) |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total | Accessories |
|  | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $2.16^{\prime \prime}$ | 1525 | $5390 /-597$ | $6915 /-$ <br> 597 | Blocking |
|  | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $3.31^{\prime \prime}$ | 2723 | 7866 | 10589 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $20^{\prime} 10^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $20^{\prime} 10^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

|  |  |  | Fead | Floor Live |  |
| :--- | :---: | :---: | :---: | :---: | :--- |
| Vertical Loads | Location (Side) | Tributary Width | $\mathbf{( 0 . 9 0 )}$ | $\mathbf{( 1 . 0 0 )}$ | Comments |
| 0 - Self Weight (PLF) | 0 to $20^{\prime} 10^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 16.8 | -- |  |
| 1- Uniform (PSF) | 0 to $15^{\prime} 10^{\prime \prime}$ (Front) | $17^{\prime}$ | 12.0 | 40.0 | Default Load |
| 2 - Point (Ib) | $20^{\prime} 77^{\prime \prime}$ (Front) | $\mathrm{N} / \mathrm{A}$ | 334 | 946 |  |
| 3 - Point (Ib) | $20^{\prime} 77^{\prime \prime}$ (Front) | $\mathrm{N} / \mathrm{A}$ | 334 | 946 |  |

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## Level, Deck Beam B5

1 piece(s) 3 1/8" $\times 18^{\prime \prime}$ 24F-V4 DF Glulam


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $3024 @ 9^{\prime} 31 / 4^{\prime \prime}$ | 7305 (5.50") | Passed (41\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $1205 @ 7^{\prime} 61 / 2^{\prime \prime}$ | 9938 | Passed (12\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Pos Moment (Ft-lbs) | $2550 @ 17^{\prime} 111 / 4^{\prime \prime}$ | 33750 | Passed (8\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (Alt Spans) |
| Neg Moment (Ft-lbs) | -3459 @ $9^{\prime} 31 / 4^{\prime \prime}$ | 26016 | Passed (13\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.024 @ 17^{\prime} 23 / 1^{\prime \prime}$ | 0.368 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (Alt Spans) |
| Total Load Defl. (in) | $0.031 @ 17^{\prime} 37 / 16^{\prime \prime}$ | 0.736 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (Alt Spans) |

System : Floor Member Type : Flush Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length $L=12^{\prime} 19 / 16^{\prime \prime}$.
- Critical negative moment adjusted by a volume factor of 1.00 that was calculated using length $L=5^{\prime} 115 / 8^{\prime \prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1 - Hanger on $18^{\prime \prime}$ DF beam | 5.50" | Hanger ${ }^{1}$ | 1.50 " | 292 | 979/-92 | $\begin{gathered} 1271 /- \\ 92 \end{gathered}$ | See note ${ }^{1}$ |
| 2-Beam-SPF | $5.50{ }^{\prime \prime}$ | 5.50" | 2.28" | 838 | 2186 | 3024 | None |
| 3 - Hanger on $18^{\prime \prime}$ DF beam | 5.50" | Hanger ${ }^{1}$ | 1.50 " | 231 | 667/-8 | 898/-8 | See note ${ }^{1}$ |

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- 1 See Connector grid below for additional information and/or requirements.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $23^{\prime} 7^{\prime \prime} 0 / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $23^{\prime} 7^{\prime \prime} 0 / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Connector: Simpson Strong-Tie |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |
| 1 - Face Mount Hanger | LGU3.25-SDS H=18 | 4.50" | N/A | 16-SDS25212 | 12-SDS25212 |  |
| 3 - Face Mount Hanger | LGU3.25-SDS H=18 | 4.50 " | N/A | 16-SDS25212 | 12-SDS25212 |  |

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

|  |  |  | Dead | Floor Live |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Vertical Loads | Location (Side) | Tributary Width | $\mathbf{( 0 . 9 0 )}$ | $\mathbf{( 1 . 0 0 )}$ | Comments |
| 0 - Self Weight (PLF) | $51 / 2^{\prime \prime}$ to $24^{\prime}$ | N/A | 13.7 | -- |  |
| 1 - Uniform (PSF) | 0 to $24^{\prime} 51 / 2^{\prime \prime}($ Top) | $2^{\prime} 6^{\prime \prime}$ | 10.0 | 40.0 | Default Load |
| 2 - Uniform (PSF) | 0 to $9^{\prime} 6^{\prime \prime}($ Back $)$ | $3^{\prime}$ | 15.0 | 40.0 |  |


| ForteWEB Software Operator | Job Notes |
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## 1 piece(s) 5 1/8" x 13 1/2" 24F-V4 DF Glulam



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 5311 @ 12' $51 / 2^{\prime \prime}$ | 5311 (1.59") | Passed (100\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | 4477 @ 11' 4" | 12223 | Passed (37\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Pos Moment (Ft-lbs) | 16680 @ 7' ${ }^{\prime \prime}$ | 31134 | Passed (54\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | 0.051 @ 6' 8" | 0.300 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | 0.225 @ 6' $67 / 16^{\prime \prime}$ | 0.600 | Passed (L/640) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Floor Member Type : Flush Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length $L=12^{\prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1 - Hanger on $131 / 2^{\prime \prime}$ DF beam | 5.50" | Hanger ${ }^{1}$ | $1.50{ }^{\prime \prime}$ | 4332 | 975 | 5307 | See note ${ }^{1}$ |
| 2 - Hanger on $131 / 2^{\prime \prime}$ DF beam | 5.50" | Hanger ${ }^{1}$ | 1.59" | 4456 | 1187 | 5643 | See note ${ }^{1}$ |

At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger

- ${ }^{1}$ See Connector grid below for additional information and/or requirements.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $12^{\prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $12^{\prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Connector: Simpson Strong-Tie |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |
| 1- Face Mount Hanger | HUCQ5.25/11-SDS | $3.00^{\prime \prime}$ | N/A | 14-SDS25212 | 6 -SDS25212 |  |
| 2 - Face Mount Hanger | HGUS5.25/10 | $4.00^{\prime \prime}$ | N/A | $46-10 d$ | $16-10 d$ |  |

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | $51 / 2^{\prime \prime}$ to $12^{\prime} 51 / 2^{\prime \prime}$ | N/A | 16.8 | -- |  |
| 1 - Uniform (PSF) | 0 to $12^{\prime} 11^{\prime \prime}$ (Front) | $2^{\prime} 6^{\prime \prime}$ | 250.0 | 40.0 | Default Load |
| 2 - Point (Ib) | $7^{\prime} 11^{\prime \prime}$ (Front) | N/A | 513 | 871 |  |
| 3 - Point (lb) | 0 (Front) | N/A | - | - |  |

## 1 piece(s) 3 1/8" x 13 1/2" 24F-V4 DF Glulam



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | 1322 @ $51 / 2^{\prime \prime}$ | $3047(1.50$ ") | Passed (43\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | 1142 @ $1^{\prime} 7^{\prime \prime}$ | 7453 | Passed (15\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Pos Moment (Ft-Ibs) | 5454 @ $8^{\prime} 81 / 2^{\prime \prime}$ | 18984 | Passed (29\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Live Load Defl. (in) | 0.145 @ $8^{\prime} 81 / 2^{\prime \prime}$ | 0.412 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Total Load Defl. (in) | 0.232 @ $8^{\prime} 81 / 2^{\prime \prime}$ | 0.825 | Passed (L/854) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |

System : Floor Member Type : Flush Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length $L=16^{\prime} 6^{\prime \prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

|  | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supports | Total | Available | Required | Dead | Floor Live | Total |  |
| 1 - Hanger on $131 / 2^{\prime \prime}$ DF beam | $5.50{ }^{\prime \prime}$ | Hanger ${ }^{1}$ | 1.50 " | 520 | 871 | 1391 | See note ${ }^{1}$ |
| 2 - Hanger on $131 / 2^{\prime \prime}$ DF beam | $5.50{ }^{\prime \prime}$ | Hanger ${ }^{1}$ | 1.50 " | 520 | 871 | 1391 | See note ${ }^{1}$ |

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $16^{\prime} 6^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $16^{\prime} 6^{\prime \prime} \circ / \mathrm{c}$ |  |

- Maximum allowable bracing intervals based on applied load.

| Connector: Simpson Strong-Tie |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |  |
| 1- Face Mount Hanger | LUS210-2 | $2.00^{"}$ | N/A | $8-10 \mathrm{dx} \times 1.5$ | $6-10 \mathrm{~d}$ |  |  |
| 2 - Face Mount Hanger | LUS210-2 | $2.00^{"}$ | $\mathrm{~N} / \mathrm{A}$ | $8-10 \mathrm{dx} \times 1.5$ |  |  |  |

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | $51 / 2^{\prime \prime}$ to $16^{\prime} 111 / 2^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 10.3 | -- |  |
| 1 - Uniform (PSF) | 0 to $17^{\prime} 5^{\prime \prime}$ (Front) | $2^{\prime} 6^{\prime \prime}$ | 20.0 | 40.0 | Default Load |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
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| Coulter Architects PLLC |  |
| (509) 630-5518 |  |
| rkent.architecture@gmail.com |  | ForteWEB v3.2, Engine: V8.2.0.17, Data: V8.1.0.16

File Name: Dave's House

## 1 piece(s) 3 1/8" x 13 1/2" 24F-V4 DF Glulam



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (Ibs) | 4779 @ $51 / 2^{\prime \prime}$ | $4779\left(2.355^{\prime \prime}\right)$ | Passed (100\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $3952 @ 1^{\prime} 7^{\prime \prime}$ | 7453 | Passed (53\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Pos Moment (Ft-lbs) | 15532 @ $6^{\prime} 111 / 2^{\prime \prime}$ | 18984 | Passed (82\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Live Load Defl. (in) | 0.056 @ $6^{\prime} 111 / 2^{\prime \prime}$ | 0.325 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Total Load Defl. (in) | $0.410 @ 6^{\prime} 111 / 2^{\prime \prime}$ | 0.650 | Passed (L/381) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |

System : Floor Member Type : Flush Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length $L=13^{\prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total | Accessories |
| 1- Hanger on $131 / 2^{\prime \prime}$ DF beam | $5.50^{\prime \prime}$ | Hanger $^{1}$ | $2.35^{\prime \prime}$ | 4416 | 696 | 5112 | See note ${ }^{1}$ |
| 2 - Hanger on $131 / 2^{\prime \prime}$ DF beam | $5.50^{\prime \prime}$ | Hanger $^{1}$ | $2.35^{\prime \prime}$ | 4416 | 696 | 5112 | See note $^{1}$ |

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $13^{\prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $13^{\prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Connector: Simpson Strong-Tie |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |  |
| 1- Face Mount Hanger | HHUS210-2 | $3.00^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | $30-16 \mathrm{~d}$ | $10-16 \mathrm{~d}$ |  |  |
| 2 - Face Mount Hanger | HHUS210-2 | $3.00^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | $30-16 \mathrm{~d}$ | $10-16 \mathrm{~d}$ |  |  |

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | $51 / 2^{\prime \prime}$ to $13^{\prime} 51 / 2^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 10.3 | -- |  |
| 1 - Uniform (PSF) | 0 to $13^{\prime} 11^{\prime \prime}$ (Front) | $2^{\prime} 6^{\prime \prime}$ | 250.0 | 40.0 | Default Load |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 6750 @ 2" | 7656 (3.50") | Passed (88\%) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{Lr}$ (All Spans) |
| Shear (lbs) | 6511 @ 1' 3/4" | 7689 | Passed (85\%) | 1.25 | $1.0 \mathrm{D}+1.0 \mathrm{Lr}$ (All Spans) |
| Moment (Ft-lbs) | 10329 @ 1' 9" | 14005 | Passed (74\%) | 1.25 | $1.0 \mathrm{D}+1.0 \mathrm{Lr}$ (All Spans) |
| Live Load Defl. (in) | 0.180 @ 4' 1/16" | 0.275 | Passed (L/549) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{Lr}$ (All Spans) |
| Total Load Defl. (in) | 0.272 @ 3' $1115 / 16^{\prime \prime}$ | 0.412 | Passed (L/364) | -- | 1.0 D + 0.75 L + 0.75 Lr (All Spans) |

System : Floor
Member Type : Drop Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: $\mathrm{LL}(L / 360)$ and $T L(L / 240)$.
- Allowed moment does not reflect the adjustment for the beam stability factor.

|  | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supports | Total | Available | Required | Dead | Floor Live | Roof Live | Total |  |
| 1 - Stud wall - DF | 3.50 " | $3.50{ }^{\prime \prime}$ | 3.09" | 2321 | 1588 | 4318 | 8227 | Blocking |
| 2 - Stud wall - DF | 3.50 " | 3.50 " | 1.50 " | 945 | 1588 | 1025 | 3558 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $8^{\prime} 7^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $8^{\prime} 7^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | $\begin{gathered} \text { Dead } \\ (0.90) \end{gathered}$ | Floor Live $(1.00)$ | Roof Live <br> (non-snow: 1.25) | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 - Self Weight (PLF) | 0 to $8^{\prime} 7^{\prime \prime}$ | N/A | 9.4 | -- | -- |  |
| 1 - Uniform (PSF) | 0 to $8^{\prime} 7^{\prime \prime}$ (Front) | $9^{1} 3^{\prime \prime}$ | 12.0 | 40.0 | - | Default Load |
| 2 - Point (lb) | 1' 9"' (Front) | N/A | 2233 | - | 5343 |  |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $977 @ 0$ | $3938(1.50 ")$ | Passed (25\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (Ibs) | $834 @ 103 / 4^{\prime \prime}$ | 6151 | Passed (14\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $2991 @ 6^{\prime} 11 / 2^{\prime \prime}$ | 11204 | Passed (27\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Live Load Defl. (in) | $0.116 @ 6^{\prime} 11 / 2^{\prime \prime}$ | 0.408 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | $0.186 @ 6^{\prime} 11 / 2^{\prime \prime}$ | 0.613 | Passed (L/792) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

System : Wall
Member Type : Header Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  |  | Loads to Supports (lbs) |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |
|  | Total | Available | Required | Dead | Floor Live | Total | Accessories |
| 1- Trimmer - DF | $1.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 364 | 613 | 977 | None |
| 2-Trimmer - DF | $1.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 364 | 613 | 977 | None |


| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $12^{\prime} 3^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $12^{\prime} 3^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

- Maximum allowable bracing intervals based on applied load.

|  |  |  | Dead | Floor Live |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Vertical Loads | Location | Tributary Width | $\mathbf{( 0 . 9 0 )}$ | $\mathbf{( 1 . 0 0 )}$ | Comments |
| 0 - Self Weight (PLF) | 0 to $12^{\prime} 3^{\prime \prime}$ | N/A | 9.4 | -- |  |
| 1 - Uniform (PSF) | 0 to $12^{\prime} 3^{\prime \prime}$ | $2^{\prime} 6^{\prime \prime}$ | 20.0 | 40.0 | Default Load |

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|  |  |



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 7561 @ 2" | 11211 (3.50") | Passed (67\%) | -- | 1.0 D + 1.0 S (All Spans) |
| Shear (lbs) | 6141 @ 1'91/2" | 18742 | Passed (33\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |
| Pos Moment (Ft-lbs) | 34823 @ 9' $61 / 2^{\prime \prime}$ | 61820 | Passed (56\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |
| Live Load Defl. (in) | 0.347 @ 9' $61 / 2^{\prime \prime}$ | 0.625 | Passed (L/648) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Total Load Defl. (in) | 0.492 @ 9' $61 / 2^{\prime \prime}$ | 0.938 | Passed (L/458) | -- | 1.0 D +1.0 S (All Spans) |

System : Floor
Member Type : Drop Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 0.97 that was calculated using length $L=18^{\prime} 99^{\prime \prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  |  | Loads to Supports (lbs) |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  |  |  |  |  |  |  |  |
|  | Total | Available | Required | Dead | Snow | Total | Accessories |
| 1 - Stud wall - DF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $2.36^{\prime \prime}$ | 2218 | 5343 | 7561 | Blocking |
| 2 - Stud wall - DF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $2.36^{\prime \prime}$ | 2218 | 5343 | 7561 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $19^{\prime} 1^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $19^{\prime} 1^{\prime \prime}$ o/c |  |

-Maximum allowable bracing intervals based on applied load.

|  |  |  | Dead | Snow |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Vertical Loads | Location (Side) | Tributary Width | $\mathbf{( 0 . 9 0 )}$ | (1.15) | Comments |
| 0 - Self Weight (PLF) | 0 to $19^{\prime} 1^{\prime \prime}$ | N/A | 22.4 | -- |  |
| 1 - Uniform (PSF) | 0 to $19^{\prime} 1^{\prime \prime}$ (Front) | $14^{\prime}$ | 15.0 | 40.0 | Default Load |

## Weyerhaeuser Notes




 and/or tested in accordance with applicable ASTM standards. For current code evaluation reports, Weyerhaeuser product literature and installation details refer to www.weyerhaeuser.com/woodproducts/document-library.
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## 2 piece(s) 1 3/4" x 9 1/2" 2.0E Microllam® LVL



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | 1318 @ $51 / 2^{\prime \prime}$ | $3938(1.50 ")$ | Passed (33\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $1191 @ 1^{\prime} 3^{\prime \prime}$ | 6318 | Passed (19\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Moment (Ft-lbs) | 5435 @ $8^{\prime} 81 / 2^{\prime \prime}$ | 11775 | Passed (46\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Live Load Defl. (in) | $0.345 @ 8^{\prime} 81 / 2^{\prime \prime}$ | 0.412 | Passed (L/574) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Total Load Defl. (in) | 0.551 @ $8^{\prime} 81 / 2^{\prime \prime}$ | 0.825 | Passed (L/359) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |

System : Floor Member Type : Flush Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

|  | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supports | Total | Available | Required | Dead | Floor Live | Total |  |
| 1-Hanger on $91 / 2^{\prime \prime}$ DF beam | 5.50 " | Hanger ${ }^{1}$ | 1.50 " | 515 | 871 | 1386 | See note ${ }^{1}$ |
| 2 - Hanger on $91 / 2^{\prime \prime}$ DF beam | 5.50 " | Hanger ${ }^{1}$ | $1.50{ }^{\prime \prime}$ | 515 | 871 | 1386 | See note ${ }^{1}$ |

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $16^{\prime} 6^{\prime \prime} \mathrm{o} / \mathrm{C}$ |  |
| Bottom Edge (Lu) | $16^{\prime} 6^{\prime \prime} \circ / \mathrm{c}$ |  |

- Maximum allowable bracing intervals based on applied load.

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | $51 / 2^{\prime \prime}$ to $16^{\prime} 111 / 2^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 9.7 | -- |  |
| 1 - Uniform (PSF) | 0 to $17^{\prime} 5^{\prime \prime}$ (Front) | $2^{\prime} 6^{\prime \prime}$ | 20.0 | 40.0 | Default Load |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
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| rkent.architecture@gmail.com |  |



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $5080 @ 11 / 2^{\prime \prime}$ | $7875\left(3.00^{\prime \prime}\right)$ | Passed (65\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Shear (Ibs) | $4152 @ 1^{\prime} 21 / 4^{\prime \prime}$ | 8603 | Passed (48\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Moment (Ft-lbs) | $15880 @ 6^{\prime} 6^{\prime \prime}$ | 18558 | Passed (86\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Live Load Defl. (in) | $0.434 @ 6^{\prime} 6^{\prime \prime}$ | 0.425 | Passed (L/352) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Total Load Defl. (in) | $0.606 @ 6^{\prime} 6^{\prime \prime}$ | 0.637 | Passed (L/253) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |

System : Wall
Member Type : Header Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Roof Live | Snow | Total |  |
| 1 - Trimmer - DF | 3.00 " | 3.00 " | 1.94" | 1440 | 3640 | 3640 | 8720 | None |
| 2 - Trimmer - DF | 3.00 " | 3.00 " | 1.94" | 1440 | 3640 | 3640 | 8720 | None |


| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $6^{\prime} 4^{\prime \prime} \circ / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $13^{\prime} \circ / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

|  |  |  | Read | Roof Live | Snow | (1.15) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Vertical Loads | Location | Tributary Width | $\mathbf{( 0 . 9 0 )}$ | (non-snow: 1.25) | Coments |  |
| 0 - Self Weight (PLF) | 0 to $13^{\prime}$ | $\mathrm{N} / \mathrm{A}$ | 11.5 | -- | -- |  |
| 1 - Uniform (PSF) | 0 to $13^{\prime}$ | $14^{\prime}$ | 15.0 | 40.0 | 40.0 | Default Load |

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|  |  |



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 3614 @ 0 | 3938 (1.50") | Passed (92\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | 2784 @ 1'3/4" | 8603 | Passed (32\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |
| Moment (Ft-lbs) | 8358 @ 4' $71 / 2^{\prime \prime}$ | 18558 | Passed (45\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | 0.129 @ 4' $71 / 2^{\prime \prime}$ | 0.308 | Passed (L/863) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Total Load Defl. (in) | 0.179 @ 4' 7 1/2" | 0.463 | Passed (L/619) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |

System : Wall
Member Type : Header Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- | :--- |
|  | Total | Available | Required | Dead | Roof Live | Snow | Total | Accessories |
| 1- Trimmer - DF | $1.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 1024 | 2590 | 2590 | 6204 | None |
| 2 - Trimmer - DF | $1.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 1024 | 2590 | 2590 | 6204 | None |


| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $9^{\prime} 33^{\prime \prime} 0 / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $9^{\prime} 3 \prime \prime / \mathrm{c}$ |  |

- Maximum allowable bracing intervals based on applied load.

|  |  |  | Dead | Roof Live | Snow |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Vertical Loads | Location | Tributary Width | $(\mathbf{0 . 9 0 )}$ | (non-snow: 1.25) | (1.15) | Comments |
| 0 - Self Weight (PLF) | 0 to $9^{\prime} 3^{\prime \prime}$ | $N / A$ | 11.5 | -- | - |  |
| 1 - Uniform (PSF) | 0 to $9^{\prime} 3^{\prime \prime}$ | $14^{\prime}$ | 15.0 | 40.0 | 40.0 | Default Load |

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| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $2297 @ 0$ | $2813\left(1.50^{\prime \prime}\right)$ | Passed (82\%) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Shear (lbs) | $1639 @ 103 / 4^{\prime \prime}$ | 3830 | Passed (43\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Momber : Wall |  |  |  |  |  |
| Member Type : Header |  |  |  |  |  |
| Building Use : Residential |  |  |  |  |  |
| Building Code : IBC 2015 |  |  |  |  |  |
| Design Methodology : ASD |  |  |  |  |  |
| Live Load Defl. (in) | $3589 @ 3^{\prime} 11 / 2^{\prime \prime}$ | 4510 | Passed (80\%) | 1.15 | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Total Load Defl. (in) | $0.057 @ 3^{\prime} 11 / 2^{\prime \prime}$ | 0.208 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

|  | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supports | Total | Available | Required | Dead | Roof Live | Snow | Total |  |
| 1 - Trimmer - DF | $1.50{ }^{\prime \prime}$ | 1.50 " | 1.50 " | 547 | 1750 | 1750 | 4047 | None |
| 2 - Trimmer - DF | 1.50" | $1.50{ }^{\prime \prime}$ | 1.50 " | 547 | 1750 | 1750 | 4047 | None |


| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $6^{\prime} 3^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $6^{\prime} 3^{\prime \prime} o / c$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location | Tributary Width | Dead <br> $(\mathbf{0 . 9 0})$ | Roof Live <br> (non-snow: $\mathbf{1 . 2 5 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $6^{\prime} 3^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 7.0 | - | - |  |
| 1 - Uniform (PSF) | 0 to $6^{\prime} 3^{\prime \prime}$ | $14^{\prime}$ | 12.0 | 40.0 | 40.0 | Default Load |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 1559 @ 0 | 2813 (1.50") | Passed (55\%) | -- | 1.0 D + 1.0 S (All Spans) |
| Shear (lbs) | 1024 @ $83 / 4^{\prime \prime}$ | 3002 | Passed (34\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |
| Moment (Ft-lbs) | 1656 @ $2^{\prime} 11 / 2^{\prime \prime}$ | 3022 | Passed (55\%) | 1.15 | 1.0 D + 1.0 S (All Spans) |
| Live Load Defl. (in) | 0.025 @ $2^{\prime} 11 / 2^{\prime \prime}$ | 0.142 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Total Load Defl. (in) | 0.033 @ 2' 11/2" | 0.213 | Passed (L/999+) | -- | 1.0 D + 1.0 S (All Spans) |

System : Wall Member Type : Header Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- | :--- |
|  | Total | Available | Required | Dead | Roof Live | Snow | Total | Accessories |
| 1-Trimmer - DF | $1.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 369 | 1190 | 1190 | 2749 | None |
| 2 - Trimmer - DF | $1.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 369 | 1190 | 1190 | 2749 | None |


| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $4^{\prime} 3^{\prime \prime} \circ / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $4^{\prime} 3^{\prime \prime} \circ / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Roof Live <br> (non-snow: $\mathbf{1 . 2 5 )}$ | Snow <br> $\mathbf{( 1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $4^{\prime} 3^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 5.5 | - | - |  |
| 1 - Uniform (PSF) | 0 to $4^{\prime} 3^{\prime \prime}$ | $14^{\prime}$ | 12.0 | 40.0 | 40.0 | Default Load |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | 1317 @ 0 | $2813\left(1.50{ }^{\prime \prime}\right)$ | Passed (47\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | $1010 @ 83 / 4^{\prime \prime}$ | 3002 | Passed (34\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Moment (Ft-lbs) | $2058 @ 3^{\prime} 11 / 2^{\prime \prime}$ | 3022 | Passed (68\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | 0.068 @ $3^{\prime} 11 / 2^{\prime \prime}$ | 0.208 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |
| Total Load Defl. (in) | $0.089 @ 3^{\prime} 11 / 2^{\prime \prime}$ | 0.313 | Passed (L/839) | -- | $1.0 \mathrm{D}+1.0$ S (All Spans) |

System : Wall
Member Type : Header Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

|  | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supports | Total | Available | Required | Dead | Roof Live | Snow | Total |  |
| 1 - Trimmer - DF | $1.50{ }^{\prime \prime}$ | 1.50 " | $1.50{ }^{\prime \prime}$ | 317 | 1000 | 1000 | 2317 | None |
| 2 - Trimmer - DF | 1.50 " | 1.50 " | $1.50{ }^{\prime \prime}$ | 317 | 1000 | 1000 | 2317 | None |


| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $6^{\prime} 3^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $6^{\prime} 3^{\prime \prime}$ o/c |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Roof Live <br> (non-snow: $\mathbf{1 . 2 5 )}$ | Snow <br> $\mathbf{( 1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 - Self Weight (PLF) | 0 to $6^{\prime} 3^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 5.5 | - | -- |  |
| 1 - Uniform (PSF) | 0 to $6^{\prime} 3^{\prime \prime}$ | $8^{\prime}$ | 12.0 | 40.0 | 40.0 | Default Load |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System : Wall <br> Member Type : Header <br> Building Use : Residential <br> Building Code : IBC 2015 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 3314 @ 11/2" | 7875 (3.00") | Passed (42\%) | -- | 1.0 D +1.0 S (All Spans) |  |
| Shear (lbs) | 2502 @ 1' 1/2" | 7265 | Passed (34\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |  |
| Moment (Ft-lbs) | 6634 @ 4' 3' | 13541 | Passed (49\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) | Design Methodology : ASD |
| Live Load Defl. (in) | 0.133 @ 4' ${ }^{\prime \prime}$ | 0.275 | Passed (L/743) | -- | 1.0 D + 1.0 S (All Spans) |  |
| Total Load Defl. (in) | 0.185 @ 4' ${ }^{\prime \prime}$ | 0.412 | Passed (L/534) | -- | 1.0 D + 1.0 S (All Spans) |  |

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Roof Live | Snow | Total |  |
| 1 - Trimmer - DF | 3.00 " | 3.00 " | 1.50 " | 934 | 2380 | 2380 | 5694 | None |
| 2 - Trimmer - DF | 3.00 " | 3.00 " | 1.50" | 934 | 2380 | 2380 | 5694 | None |


| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $8^{\prime} 6^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $8^{\prime} 6^{\prime \prime} \mathrm{o} / \mathrm{C}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Roof Live <br> (non-snow: $\mathbf{1 . 2 5 )}$ | Snow <br> (1.15) | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | 0 to $8^{\prime} 6^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 9.7 | -- | -- |  |
| 1 - Uniform (PSF) | 0 to $8^{\prime} 6^{\prime \prime}$ | $14^{\prime}$ | 15.0 | 40.0 | 40.0 | Default Load |

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Existing House, Deck Beam B12
1 piece(s) 3 1/8" x 18" 24F-V8 DF Glulam


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) | System : Floor <br> Member Type : Flush Beam <br> Building Use : Residential <br> Building Code : IBC 2015 <br> Design Methodology : ASD |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 1757 @ 4" | 8301 (4.25") | Passed (21\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |  |
| Shear (lbs) | 1442 @ 1'11 1/2" | 9938 | Passed (15\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |  |
| Pos Moment (Ft-lbs) | 8697 @ 10' $51 / 2^{\prime \prime}$ | 33750 | Passed (26\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |  |
| Live Load Defl. (in) | 0.166 @ 10' $51 / 2^{\prime \prime}$ | 0.506 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |  |  |
| Total Load Defl. (in) | 0.235 @ 10' $51 / 2^{\prime \prime}$ | 1.013 | Passed (L/999+) | -- | 1.0 D + 1.0 L (All Spans) |  |  |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length $L=20^{\prime} 3^{\prime \prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- Applicable calculations are based on NDS

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total | Accessories |
| 1-Stud wall - DF | $5.50^{\prime \prime}$ | $4.25^{\prime \prime}$ | $1.50^{\prime \prime}$ | 518 | 1255 | 1773 | $11 / 4^{\prime \prime}$ Rim Board |
| 2 - Stud wall - DF | $5.50^{\prime \prime}$ | $4.25^{\prime \prime}$ | $1.50^{\prime \prime}$ | 518 | 1255 | 1773 | $11 / 4^{\prime \prime}$ Rim Board |


| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $20^{\prime} 9^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $20^{\prime} 9^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $(\mathbf{0 . 9 0})$ | Floor Live <br> $(\mathbf{1 . 0 0})$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | $11 / 4^{\prime \prime}$ to $20^{\prime} 93 / 4^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 13.7 | -- |  |
| 1 - Uniform (PSF) | 0 to $20^{\prime} 11^{\prime \prime}$ (Front) | $3^{\prime}$ | 12.0 | 40.0 | Default Load |

## Weyerhaeuser Notes




 and/or tested in accordance with applicable ASTM standards. For current code evaluation reports, Weyerhaeuser product literature and installation details refer to www.weyerhaeuser.com/woodproducts/document-library.
The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $2875 @ 10^{\prime} 51 / 4^{\prime \prime}$ | $7623\left(3.50^{\prime \prime}\right)$ | Passed (38\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{Lr}$ (All Spans) |
| Shear (lbs) | 1893 @ $9^{\prime} 5^{\prime \prime}$ | 11884 | Passed (16\%) | 1.25 | $1.0 \mathrm{D}+1.0 \mathrm{Lr}$ (All Spans) |
| Pos Moment (Ft-lbs) | 5871 @ $5^{\prime} 31 / 16^{\prime \prime}$ | 23543 | Passed (25\%) | 1.25 | $1.0 \mathrm{D}+1.0 \mathrm{Lr}$ (Alt Spans) |
| Neg Moment (Ft-lbs) | $-297 @ 10^{\prime} 51 / 4^{\prime \prime}$ | 23543 | Passed (1\%) | 1.25 | $1.0 \mathrm{D}+1.0 \mathrm{Lr}$ (All Spans) |
| Live Load Defl. (in) | $0.076 @ 5^{\prime} 31 / 2^{\prime \prime}$ | 0.514 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{Lr}$ (Alt Spans) |
| Total Load Defl. (in) | $0.125 @ 5^{\prime} 37 / 16^{\prime \prime}$ | 0.685 | Passed (L/987) | -- | $1.0 \mathrm{D}+1.0 \mathrm{Lr}$ (Alt Spans) |

System : Roof Member Type : Drop Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: LL (2L/240) and TL (2L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length $L=10^{\prime} 23 / 16^{\prime \prime}$.
- Critical negative moment adjusted by a volume factor of 1.00 that was calculated using length $L=1^{\prime} 35 / 16^{\prime \prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  |  | Loads to Supports (Ibs) |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Roof Live | Total | Accessories |
|  | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 933 | 1449 | 2382 | Blocking |
| 2 - Stud wall - SPF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 1130 | 1745 | 2875 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $11^{\prime} 77^{\prime \prime} \circ / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $11^{\prime} 7^{\prime \prime} \circ / \mathrm{C}$ |  |

- Maximum allowable bracing intervals based on applied load.

|  |  |  | Read | Roof Live |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Vertical Loads | Location (Side) | Tributary Width | $\mathbf{( 0 . 9 0 )}$ | (non-snow: 1.25) | Comments |
| 0 - Self Weight (PLF) | 0 to $11^{\prime} 7^{\prime \prime}$ | N/A | 13.1 | -- |  |
| 1 - Uniform (PSF) | 0 to $11^{\prime} 7^{\prime \prime}$ (Front) | $11^{\prime}$ | 15.0 | 25.0 | Default Load |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | 2867 @ 4" | $13613\left(4.25^{\prime \prime}\right)$ | Passed (21\%) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{Lr}$ (All Spans) |
| Shear (lbs) | 2248 @ $1^{\prime} 10^{\prime \prime}$ | 14939 | Passed (15\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Pos Moment (Ft-lbs) | 22457 @ $11^{\prime} 51 / 2^{\prime \prime}$ | 55990 | Passed (40\%) | 1.25 | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{Lr}$ (All Spans) |
| Live Load Defl. (in) | $0.294 @ 11^{\prime} 51 / 2^{\prime \prime}$ | 0.556 | Passed (L/908) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{Lr}$ (All Spans) |
| Total Load Defl. (in) | $0.510 @ 11^{\prime} 51 / 2^{\prime \prime}$ | 1.112 | Passed (L/523) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{Lr}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 0.96 that was calculated using length $L=22^{\prime} 3^{\prime \prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Roof Live | Total |  |
| 1-Stud wall - DF | $5.50{ }^{\prime \prime}$ | 4.25" | 1.50 " | 1195 | 1375 | 873 | 3443 | 11/4" Rim Board |
| 2 - Stud wall - DF | 5.50" | 4.25" | 1.50 " | 1195 | 1375 | 873 | 3443 | 11/4" Rim Board |

- Rim Board is assumed to carry all loads applied directly above it, bypassing the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $22^{\prime \prime} 9^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $22^{\prime \prime} 9^{\prime \prime} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $\mathbf{( 1 . 0 0 )}$ | Roof Live <br> (non-snow: 1.25) | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | $11 / 4^{\prime \prime}$ to $22^{\prime} 93 / 4^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 20.5 | - | -- |  |
| 1 - Uniform (PSF) | 0 to $22^{\prime} 11^{\prime \prime}$ (Front) | $3^{\prime}$ | 12.0 | 40.0 | - | Default Load |
| 2 - Point (lb) | $11^{\prime} 51 / 2^{\prime \prime}$ (Front) | $\mathrm{N} / \mathrm{A}$ | 1098 | - | 1745 |  |

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Existing House, Deck Beam B15
2 piece(s) 1 3/4" x 18" 2.0E Microllam® LVL


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | 934 @ $4^{\prime \prime}$ | $9297\left(4.25^{\prime \prime}\right)$ | Passed (10\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (lbs) | $610 @ 1^{\prime} 111 / 2^{\prime \prime}$ | 11970 | Passed (5\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | 2290 @ $5^{\prime} 51 / 2^{\prime \prime}$ | 38753 | Passed (6\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Live Load Defl. (in) | 0.012 @ $5^{\prime} 51 / 2^{\prime \prime}$ | 0.256 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |
| Total Load Defl. (in) | $0.017 @ 5^{\prime} 51 / 2^{\prime \prime}$ | 0.512 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0$ L (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

| Supports | Bearing Length |  |  |  | Loads to Supports (Ibs) |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

- Rim Board is assumed to carry all loads applied directly above it, bypassing the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $10^{\prime} 9^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $10^{\prime} 99^{\prime \prime} \mathrm{o} \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $(\mathbf{0 . 9 0})$ | Floor Live <br> $\mathbf{( 1 . 0 0 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | $11 / 4^{\prime \prime}$ to $10^{\prime} 93 / 4^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 18.4 | -- |  |
| 1 - Uniform (PSF) | 0 to $10^{\prime} 11^{\prime \prime}$ (Front) | $3^{\prime}$ | 12.0 | 40.0 | Default Load |

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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | 2338 @ 4" | $13613\left(4.25^{\prime \prime}\right)$ | Passed (17\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Shear (Ibs) | 2007 @ $1^{\prime} 111 / 2^{\prime \prime}$ | 16298 | Passed (12\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Pos Moment (Ft-lbs) | 14788 @ $13^{\prime} 21 / 2^{\prime \prime}$ | 52078 | Passed (28\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | 0.265 @ $13^{\prime} 21 / 2^{\prime \prime}$ | 0.644 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Total Load Defl. (in) | $0.394 @ 13^{\prime} 21 / 2^{\prime \prime}$ | 1.288 | Passed (L/785) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 0.94 that was calculated using length $L=25^{\prime} 9^{\prime \prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1 - Stud wall - DF | 5.50" | 4.25" | 1.50 " | 769 | 1585 | 2354 | $11 / 4^{\prime \prime}$ Rim Board |
| 2 - Stud wall - DF | 5.50" | 4.25" | 1.50" | 769 | 1585 | 2354 | $11 / 4$ " Rim Board |

- Rim Board is assumed to carry all loads applied directly above it, bypassing the member being designed.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $26^{\prime} 3^{\prime \prime}$ o/c |  |
| Bottom Edge (Lu) | $26^{\prime} 3^{\prime \prime}$ o/c |  |

-Maximum allowable bracing intervals based on applied load.

|  |  |  | Dead | Floor Live |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Vertical Loads | Location (Side) | Tributary Width | $\mathbf{( 0 . 9 0 )}$ | $\mathbf{( 1 . 0 0 )}$ | Comments |
| 0 - Self Weight (PLF) | $11 / 4^{\prime \prime}$ to $26^{\prime} 33 / 4^{\prime \prime}$ | $N / A$ | 22.4 | -- |  |
| 1 - Uniform (PSF) | 0 to $26^{\prime} 5^{\prime \prime}$ (Front) | $3^{\prime}$ | 12.0 | 40.0 | Default Load |

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Level, Deck Beam B17
1 piece(s) 3 1/8" x 18" 24F-V4 DF Glulam


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (Ibs) | $1306 @ 51 / 2^{\prime \prime}$ | $3047\left(1.50^{\prime \prime}\right)$ | Passed (43\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (Alt Spans) |
| Shear (lbs) | $1192 @ 17^{\prime} 111 / 2^{\prime \prime}$ | 9938 | Passed (12\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Pos Moment (Ft-Ibs) | 6148 @ $9^{\prime} 101 / 2^{\prime \prime}$ | 33750 | Passed (18\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (Alt Spans) |
| Neg Moment (Ft-lbs) | $-1896 @ 19^{\prime} 81 / 4^{\prime \prime}$ | 26016 | Passed (7\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.113 @ 10^{\prime} 7 / 8^{\prime \prime}$ | 0.481 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (Alt Spans) |
| Total Load Defl. (in) | $0.148 @ 10^{\prime} 1 / 16^{\prime \prime}$ | 0.961 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0$ L (Alt Spans) |

System : Floor Member Type : Flush Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Overhang deflection criteria: LL (2L/480) and TL (2L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length $\mathrm{L}=18^{\prime} 10^{\prime \prime}$.
- Critical negative moment adjusted by a volume factor of 1.00 that was calculated using length $L=6^{\prime} 713 / 16^{\prime \prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

|  | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supports | Total | Available | Required | Dead | Floor Live | Total |  |
| 1 - Hanger on $18^{\prime \prime}$ DF beam | $5.50{ }^{\prime \prime}$ | Hanger ${ }^{1}$ | 1.50 " | 356 | 1007/-25 | $\begin{gathered} 1363 /- \\ 25 \end{gathered}$ | See note ${ }^{1}$ |
| 2 - Beam - DF | 5.50 " | 5.50" | 1.50 " | 602 | 1555 | 2157 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $24^{\prime} 6^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $24^{\prime} 6^{\prime \prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

## Connector: Simpson Strong-Tie

| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 - Face Mount Hanger | LGU3.25-SDS H=18 | $4.50^{\prime \prime}$ | N/A | $16-$ SDS25212 | $12-$ SDS 25212 |  |

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $\mathbf{( 1 . 0 0 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | $51 / 2^{\prime \prime}$ to $24^{\prime} 11^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 13.7 | -- |  |
| 1 - Uniform (PSF) | 0 to $24^{\prime} 11^{\prime \prime}$ (Front) | $2^{\prime} 6^{\prime \prime}$ | 10.0 | 40.0 | Default Load |


| ForteWEB Software Operator | Job Notes |
| :--- | :--- |
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All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (Ibs) | 1754 @ $51 / 2^{\prime \prime}$ | $3047\left(1.50^{\prime \prime}\right)$ | Passed (58\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (Alt Spans) |
| Shear (lbs) | 1546 @ $1^{\prime} 111 / 2^{\prime \prime}$ | 9938 | Passed (16\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (Alt Spans) |
| Pos Moment (Ft-lbs) | 4758 @ $4^{\prime} 57 / 16^{\prime \prime}$ | 33750 | Passed (14\%) | 1.00 | $1.0 \mathrm{D}+1.0$ L (Alt Spans) |
| Neg Moment (Ft-lbs) | $-1896 @ 13^{\prime} 21 / 4^{\prime \prime}$ | 26016 | Passed (7\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.039 @ 6^{\prime} 57 / 8^{\prime \prime}$ | 0.318 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (Alt Spans) |
| Total Load Defl. (in) | $0.048 @ 6^{\prime} 53 / 16^{\prime \prime}$ | 0.636 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0$ L (Alt Spans) |

System : Floor
Member Type : Flush Beam
Building Use : Residential
Building Code : IBC 2015
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Overhang deflection criteria: LL (2L/480) and TL (2L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length $L=12^{\prime} 33 / 8^{\prime \prime}$,
- Critical negative moment adjusted by a volume factor of 1.00 that was calculated using length $L=6^{\prime} 99 / 16^{\prime \prime}$.
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (Ibs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1 - Hanger on $18^{\prime \prime}$ DF beam | 5.50" | Hanger ${ }^{1}$ | 1.50 " | 399 | 1413/-62 | $\begin{gathered} 1812 /- \\ 62 \end{gathered}$ | See note ${ }^{1}$ |
| 2 - Beam - DF | $5.50{ }^{\prime \prime}$ | 5.50" | 1.50 " | 547 | 1496 | 2043 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.

| Lateral Bracing | Bracing Intervals | Comments |
| :--- | :---: | :--- |
| Top Edge (Lu) | $18^{\prime} \mathrm{o} / \mathrm{c}$ |  |
| Bottom Edge (Lu) | $18^{\prime} \mathrm{o} / \mathrm{c}$ |  |

-Maximum allowable bracing intervals based on applied load.

| Connector: Simpson Strong-Tie |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |
| 1- Face Mount Hanger | LGU3.25-SDS H=18 | $4.50^{\prime \prime}$ | N/A | 16 -SDS25212 | 12 -SDS25212 |  |

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

|  |  |  | Floor Live |  |  |
| :--- | :---: | :---: | :---: | :---: | :--- |
| Vertical Loads | Location (Side) | Tributary Width | (0.90) | $\mathbf{( 1 . 0 0 )}$ | Comments |
| 0 - Self Weight (PLF) | $51 / 2^{\prime \prime}$ to $18^{\prime} 5^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 13.7 | - |  |
| 1 - Uniform (PSF) | 0 to $18^{\prime} 5^{\prime \prime}$ (Front) | $2^{\prime} 6^{\prime \prime}$ | 10.0 | 40.0 | Default Load |
| 2 - Point (Ib) | $3^{\prime} 6^{\prime \prime}$ (Front) | $\mathrm{N} / \mathrm{A}$ | 240 | 960 |  |


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## COULTER ARCHITECTURE

RE: New Home for Pattie and Dave Coulter 35465 Rueppell Avenue<br>Pacific City, OR<br>Tillamook County

Design Criteria used in the design of the this structure is listed below:

## GRAVITY

| Snow Load: | 36 PSF Ground Snow Load |
| :--- | :--- |
|  | 25 PSF Roof Snow) |
| Live Load: | 40 PSF residential $\& 60$ PSF decks |
| Dead Loads: | 15 PSF or "self-weight" |

## LATERAL

## SEISMIC

Equivalent lateral force procedure per 2018 IBC and ASCE 7-16 Site Class E, Seismic Design Category is "D"

## UPPER (MAIN) LEVEL:

Systems:
Cantilevered Concrete Columns @ Carport $\rightarrow \mathrm{R}=2,5$
$\mathrm{Cs}=0.184$
Wood framed shearwalls Balance $\rightarrow \mathrm{R}=6.0$ (used 5.0 to be conservative)
$\mathrm{Cs}=0.1364$
$\mathbf{V e q}=14,720 \mathrm{lb}$ Total $\leftarrow$
WIND
WIND SPEED $=115 \mathrm{mph}, 3$ second gust (ultimate)
WIND EXPOSURE, "C"
WIND Kzt $=1.02$
$\mathrm{V}=5,862 \mathrm{lb} \mathrm{N} / \mathrm{S}$
$\mathrm{V}=11,244 \mathrm{lb} \mathrm{E} / \mathrm{W}$

## SEISMIC FORCES CONTROL LATERAL DESIGN!

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## MAIN WIND FORCE RESISTING SYSTEM

## Basic Values



User has specified the building frequency is $>=1 \mathrm{~Hz}$, therefore considered RIGID for both North-South and East-West directions.

Building Story Data

| Level Description | hi <br> ft | Story Ht <br> ft | $\mathrm{E}_{\mathrm{R}}: \mathrm{X}$ <br> ft | $\mathrm{E}_{\mathrm{R}}: \mathrm{X}$ <br> ft |
| :--- | :---: | :---: | :---: | :---: |
| ROOF | 22.00 | 11.00 | 0.000 | 0.000 |
| FLOOR | 11.00 | 11.00 | 0.000 | 0.000 |


| Gust Factor |  | For wind coming from direction indicated |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| North | $=$ | 0.850 | South | $=$ | 0.850 |
| East | $=$ | 0.850 | West | $=$ | 0.850 |

## Enclosure

Check if Building Qualifies as "Open"

|  | North Wall | South Wall | East Wall | West Wall | Roof | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Agross | $\mathrm{ft}^{\wedge} 2$ | $\mathrm{ft}^{\wedge} 2$ | $\mathrm{ft}^{\wedge} 2$ | $\mathrm{ft}^{\wedge} 2$ | $\mathrm{ft}^{\wedge} 2$ | $0.0 \mathrm{ft}^{\wedge} 2$ |
| Aopenings | $\mathrm{ft}^{\wedge} 2$ | $\mathrm{ft}^{\wedge} 2$ | $\mathrm{ft}^{\wedge} 2$ | $\mathrm{ft}^{\wedge} 2$ | $\mathrm{ft}^{\wedge} 2$ | $0.0 \mathrm{ft}^{\wedge} 2$ |
| Aopenings $>=0.8$ * Agross ? | Yes | Yes | Yes | Yes |  |  |

All four Agross values must be non-zero
Building qualifies as "Open"
North Elevation : Determine Enclosure Classification per ASCE Section 26.12

| Reference area $=$ smaller of 4 sq. ft. or $1 \%$ of Agross | $=$ | $0.0 \mathrm{ft}^{\wedge} 2$ | Is Ao $>1.10{ }^{*}$ Aoi ? | $=$ |
| :--- | :--- | :--- | :--- | :--- |
| Aoi $=$ Ao-total -Ao | $=$ | $0.0 \mathrm{f}^{\wedge} 2$ | Is Ao $>$ Reference Area? | $=$ |
| Agi $=$ Ag-total -Ag | $=$ | $0.0 \mathrm{ft}^{\wedge} 2$ | Is Aoi $/$ Agi $>=0.20 ?$ | No |
| Aoi $/$ Agi | 0.0 |  | No | Yes |

## Building is "Enclosed" when the North wall receives positive external pressure

South Elevation : Determine Enclosure Classification per ASCE Section 26.12

| Reference area $=$ smaller of 4 sq. ft. or $1 \%$ of Agross | $=$ | $0.0 \mathrm{ft}^{\wedge} 2$ | Is Ao $>1.10$ * Aoi ? | $=$ |
| :--- | :--- | :--- | :--- | :--- |
| Aoi $=$ Ao-total - Ao | $=$ | $0.0 \mathrm{f}^{\wedge} 2$ | Is Ao $>$ Reference Area? | $=$ |
| Agi $=$ Ag-total -Ag | $=$ | $0.0 \mathrm{f}^{\wedge} 2$ | Is Aoi $/$ Agi $>=0.20 ?$ | No |
| Aoi $/$ Agi | 0.0 |  | No | Yes |

## Building is "Enclosed" when the South wall receives positive external pressure

East Elevation : Determine Enclosure Classification per ASCE Section 26.12

| Reference area $=$ smaller of 4 sq. ft. or $1 \%$ of Agross | $=$ | $0.0 \mathrm{ft}^{\wedge} 2$ | Is Ao $>1.10 *$ Aoi ? | $=$ |
| :--- | :--- | :--- | :--- | :--- |
| Aoi $=$ Ao-total -Ao | $=$ | $0.0 \mathrm{f}^{\wedge} 2$ | Is Ao $>$ Reference Area? | $=$ |
| Agi $=$ Ag-total -Ag | $=$ | $0.0 \mathrm{f}^{\wedge} 2$ | Is Aoi $/$ Agi $>=0.20 ?$ | No |
| Aoi $/$ Agi | 0.0 |  | No | Yes |

Building is "Enclosed" when the East wall receives positive external pressure

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DESCRIPTION: WIND BASE SHEAR
West Elevation : Determine Enclosure Classification per ASCE Section 26.12

| Reference area $=$ smaller of 4 sq . ft. or $1 \%$ of Agross | = | $0.0 \mathrm{ff}^{\wedge} 2$ | Is $A 0>1.10$ * Aoi ? | = | No |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Aoi $=$ Ao-total - Ao | = | $0.0 \mathrm{ft}^{\wedge} 2$ | Is $A 0>$ Reference Area? | = | No |
| Agi $=$ Ag-total -Ag | = | $0.0 \mathrm{ft}^{\wedge} 2$ | Is Aoi / Agi > $=0.20$ ? |  | Yes |
| Aoi / Agi | = | 0.0 |  |  |  |

Building is "Enclosed" when the West wall receives positive external pressure

## Velocity Pressures

When the following walls experience leeward or sidewall pressures, the value of Kh shall be (per Table 26.10-1) : North Wall $=0.9245 \mathrm{psf} \quad$ South Wall $=0.9245 \mathrm{psf} \quad$ East Wall $=0.9245 \mathrm{psf} \quad$ West Wall $=\quad 0.9245$ psf
When the following walls experience leeward or sidewall pressures, the value of qh shall be (per Table 26.10-1) North Wall $=26.913$ psf $\quad$ South Wall $=26.913$ psf $\quad$ East Wall $=\quad 26.913$ psf $\quad$ West Wall $=26.913$ psf
qz : Windward Wall Velocity Pressures at various heights per Eq. 26.10-1

|  | North Elevation |  | South Elevation |  | East Elevation |  | West Elevation |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
| Height Above Base (ft) | Kz | qz | Kz | qz | Kz | qz | Kz |  |
| 0.00 | 0.849 | 24.71 | 0.849 | 24.71 | 0.849 | 24.71 | 0.849 |  |
| 5.00 | 0.849 | 24.71 | 0.849 | 24.71 | 0.849 | 24.71 | 0.849 |  |
| 10.00 | 0.849 | 24.71 | 0.849 | 24.71 | 0.849 | 24.71 | 0.849 |  |
| 15.00 | 0.849 | 24.71 | 0.849 | 24.71 | 24.71 |  |  |  |
| 20.00 | 0.902 | 26.25 | 0.902 | 26.25 | 0.849 | 24.71 | 0.849 |  |
| Pressure Coefficients |  |  |  | GCpi Values when elevation receives positive external pressure |  |  |  |  |

## Pressure Coefficients

GCpi Values when elevation receives positive external pressure
GCpi : Internal pressure coefficient, per sec. 26.13 and Table 26.13-1


Specify Cp Values from Figure 27.3-1 for Windward, Leeward \& Side Walls
Cp Values when elevation receives positive external pressure

|  | North | South | East | West |
| :---: | :---: | :---: | :---: | :---: |
| Windward Wall | 0.80 | 0.80 | 0.80 | 0.80 |
| Leeward Wall |  |  |  |  |
| Side Walls | -0.70 | -0.70 | -0.70 | -0.70 |

## Wind Pressures

Wind Pressures when NORTH Elevation receives positive external wind pressure

|  | Positive Internal | Negative Internal |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Leeward Wall Pressures | 0.0 psf |  |  |  |
| Side Wall Pressures | -16.013 psf |  |  |  |
| Windward Wall Pressures . . Height Above Base (ft) | . Positive Internal Pressure (psf) | Negative Internal Pressure (psf) |  |  |
| 0.00 |  | 16.80 |  | 16.80 |
| 5.00 |  | 16.80 |  | 16.80 |
| 10.00 |  | 16.80 |  | 16.80 |
| 15.00 |  | 16.80 |  | 16.80 |
| 20.00 |  | 17.85 |  | 17.85 |

Wind Pressures when SOUTH Elevation receives positive external wind pressure

|  | Positive Internal | Negative Internal |
| :---: | :---: | :---: |
| Leeward Wall Pressures | 0.0 psf | 0.0 psf |
| Side Wall Pressures | -16.013 psf | -16.013psf |
| Windward Wall Pressures Height Above Base (ft) | Positive Internal <br> Pressure (psf) | Negative Internal Pressure (psf) |

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| 0.00 | 16.80 | 16.80 |
| :---: | :---: | :---: |
| 5.00 | 16.80 | 16.80 |
| 10.00 | 16.80 | 16.80 |
| 15.00 | 16.80 | 16.80 |
| 20.00 | 17.85 | 17.85 |

Wind Pressures when EAST Elevation receives positive external wind pressure

|  | Positive Internal | Negative Internal |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Leeward Wall Pressures | 0.0 psf | 0.0 psf -16.013psf |  |  |
| Side Wall Pressures | -16.013 psf |  |  |  |
| Windward Wall Pressures Height Above Base (ft) | Positive Internal <br> Pressure (psf) | Negative Internal Pressure (psf) |  |  |
| 0.00 |  | 16.80 |  | 16.80 |
| 5.00 |  | 16.80 |  | 16.80 |
| 10.00 |  | 16.80 |  | 16.80 |
| 15.00 |  | 16.80 |  | 16.80 |
| 20.00 |  | 17.85 |  | 17.85 |

Wind Pressures when WEST Elevation receives positive external wind pressure

|  | Positive Internal | Negative Internal |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Leeward Wall Pressures | 0.0 psf | $\begin{array}{r} 0.0 \mathrm{psf} \\ -16.013 \mathrm{psf} \end{array}$ |  |  |
| Side Wall Pressures | -16.013 psf |  |  |  |
| Windward Wall Pressures . . . Height Above Base (ft) | . Positive Internal Pressure (psf) | Negative Internal <br> Pressure (psf) |  |  |
| 0.00 |  | 16.80 |  | 16.80 |
| 5.00 |  | 16.80 |  | 16.80 |
| 10.00 |  | 16.80 |  | 16.80 |
| 15.00 |  | 16.80 |  | 16.80 |
| 20.00 |  | 17.85 |  | 17.85 |

## Story Forces for Design Wind Load Cases

Values below are calculated based on a building with dimensions $B \times L \times h$ as defined on the "Basic Values" tab.
Wind Shear Components (k) Eccentricity for (ft)

| Load Case | Windward Wall |  | Ht. Range | Wind Shear Components (k) Eccentricity for (ft) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Windward Wall | Building level |  | Trib. Height | In "Y" Direction | In "X" Directio | Shear | "X" Shear |  | (ft-k) |
| CASE 1 | North | Level 2 | $16.50{ }^{\prime}$-> 22.00 | 5.50 | -3.60 | --- | --- | --- |  | --- |
| CASE 1 | North | Level 1 | $5.50{ }^{\prime}$-> $16.50^{\prime}$ | 11.00 | -6.85 | --- | --- | --- |  | --- |
| CASE 1 | South | Level 2 | 16.50' -> 22.00 | 5.50 | 3.60 | --- | --- | --- |  | --- |
| CASE 1 | South | Level 1 | $5.50{ }^{\prime}$-> 16.50' | 11.00 | 6.85 | --- | --- | --- |  | --- |
| CASE 1 | East | Level 2 | $16.50{ }^{\prime}$-> 22.00 | 5.50 | --- | -6.91 | --- | --- |  | --- |
| CASE 1 | East | Level 1 | $5.50{ }^{\prime}$-> $16.50{ }^{\prime}$ | 11.00 | --- | -13.14 | --- | --- |  | --- |
| CASE 1 | West | Level 2 | $16.50{ }^{\prime}$-> 22.00 | 5.50 | --- | 6.91 | --- | --- |  | --- |
| CASE 1 | West | Level 1 | 5.50 '-> 16.50' | 11.00 | --- | 13.14 | --- | --- |  | --- |
| CASE 2 | North | Level 2 | 16.50' -> 22.00 | 5.50 | -2.70 | --- | --- | $5.55+$ | +/- | 15.0 |
| CASE 2 | North | Level 1 | $5.50{ }^{\prime}$-> 16.50' | 11.00 | -5.14 | --- | --- | $5.55+$ | +/- | 28.5 |
| CASE 2 | South | Level 2 | 16.50' -> 22.00 | 5.50 | 2.70 | --- | --- | $5.55+$ | +/- | 15.0 |
| CASE 2 | South | Level 1 | 5.50 '>> 16.50' | 11.00 | 5.14 | --- | --- | $5.55+$ | +/- | 28.5 |
| CASE 2 | East | Level 2 | $16.50{ }^{\prime}$-> 22.00 | 5.50 | --- | -5.18 | 9.92 | --- + | +/- | 51.4 |
| CASE 2 | East | Level 1 | 5.50 '-> 16.50' | 11.00 | --- | -9.86 | 9.92 | --- + | +/- | 97.8 |

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Values below are calculated based on a building with dimensions B $\times \mathrm{L} \times \mathrm{h}$ as defined on the "General" tab.


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## ASCE 7-16 Wind Forces, Chapter 27, Part I

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DESCRIPTION: WIND BASE SHEAR

| Case 4 | North \& West | South \& East | -5.88 | 11.29 | $+/-$ | 144.6 |
| :--- | :---: | :---: | :---: | ---: | ---: | ---: |
| Case 4 | South \& West | North \& East | 5.88 | 11.29 | $+/-$ | 144.6 |
| Case 4 | South \& East | North \& West | 5.88 | -11.29 | $+/-$ | 144.6 |
|  |  |  |  |  |  |  |
| Min per ASCE 27.1.5 | North | South | -9.77 | --- | --- |  |
| Min per ASCE 27.1.5 | South | North | 9.77 | -- | -- |  |
| Min per ASCE 27.1.5 | East | West | --- | -18.74 | -- |  |
| Min per ASCE 27.1.5 | West | East | --- | 18.74 | --- |  |

## ASD WORKING LEVEL FORCES

NORTH SOUTH $=5,862$ LB
EAST WEST $=11,244 \mathrm{LB}$

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## Site Class, Site Coeff. and Design Category

| Site Classification "E" : Shear Wave Velocity must be less than 600 ftsec |  | = | E | ASCE 7-16 Table 20.3-1 |
| :---: | :---: | :---: | :---: | :---: |
| Site Coefficients Fa \& Fv | Fa | = | 1.00 | ASCE 7-16 Table 11.4-1 \& 11.4-2 |
| (using straight-line interpolation from table values) | Fv | = | 2.00 |  |
| Maximum Considered Earthquake Acceleration | $\begin{aligned} & S_{M S}=\mathrm{Fa}^{*} \mathrm{Ss} \\ & S_{M 1}=\mathrm{Fv}^{*} \mathrm{~S}^{2} \end{aligned}$ | = | 1.330 | ASCE 7-16 Eq. 11.4-1 |
|  |  | $=$ | 1.357 | ASCE 7-16 Eq. 11.4-2 |
| Design Spectral Acceleration | $\begin{array}{ll} S_{D S}=S & M S^{*} 2 / 3 \\ S_{D 1}=S & M_{1}^{*} 2 / 3 \end{array}$ | = | 0.887 | ASCE 7-16 Eq. 11.4-3 |
|  |  | = | 0.904 | ASCE 7-16 Eq. 11.4-4 |
| Seismic Design Category |  | = | D | ASCE 7-16 Table 11.6-1 \& -2 |
| Resisting System |  |  |  | ASCE 7-16 Table 12.2-1 |

Basic Seismic Force Resisting System .
Bearing Wall Systems
15.Light-frame (wood) walls sheathed w/wood structural panels rated for shear resistance.

| Response Modification Coefficient " R " | $=$ | 6.50 | Building height Limits : |  |
| :--- | :--- | :--- | :--- | :--- |
| System Overstrength Factor " Wo " | $=$ | 3.00 | Category "A \& B" Limit: | No Limit |
| Deflection Amplification Factor " Cd " | $=$ | 4.00 | Category "C" Limit: | No Limit |
| NOTE! See ASCE 7-16 for all applicable footnotes. |  | Category "D" Limit: | Limit =65 |  |
|  |  | Category "E" Limit: | Limit $=65$ |  |
|  |  | Category "F" Limit: | Limit $=65$ |  |

## Lateral Force Procedure

Equivalent Lateral Force Procedure
The "Equivalent Lateral Force Procedure" is being used according to the provisions of ASCE 7-16 12.8
Determine Building Period
Structure Type for Building Period Calculation: All Other Structural Systems
" Ct " value $=0.020 \quad$ " hn " : Height from base to highest level $=024.0 \mathrm{ft}$
" $x$ " value $=0.75$
" Ta " Approximate fundemental period using Eq. 12.8-7: $\quad \mathrm{Ta}=\mathrm{Ct}^{*}\left(\mathrm{hn}{ }^{\wedge} \mathrm{x}\right)=0.217 \mathrm{sec}$
"TL" : Long-period transition period per ASCE 7-16 Maps 22-14 -> 22-17
8.000 sec

Building Period " Ta " Calculated from Approximate Method selected $=0.217 \mathrm{sec}$


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ASCE Seismic Base Shear
Printed: 14 JUN 2021. 9:20AM
File: DAVE COULTER.ec6
LLic. \#: KW-06009465
DESCRIPTION: COULTER BASE SHEAR



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Project ID: 28PV21
Project Descr:Two - Story @ 35465 Rueppell Ave

Torsional Analysis of Rigid Diaphragm
Printed: 14 JUN 2021, 10:53AM
File: DAVE COULTER.ec6
Lic. \#: KW-06009465
DESCRIPTION: RELATIVE RIGIDITY FOR LOWER LEVEL
General Information
IBC 2018, CBC 2019, ASCE 7-16


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Project Title: New Home for Pattie and Dave Coulter
Engineer: $\quad \mathrm{S} / \mathrm{P}$
Project ID: 28PV21
Project Descr:Two - Story @ 35465 Rueppell Ave

Torsional Analysis of Rigid Diaphragm
Printed: 14 JUN 2021, 10:53AM
File: DAVE COULTER.ec6
Lic. \# : KW-06009465 Soffware copyright ENERCALC, INC. 1983-2020, Build:12.20.5.3

DESCRIPTION: RELATIVE RIGIDITY FOR LOWER LEVEL
Wall Information

| Label: BOAT GARAGE MIDDLE | X Wall C.G. Location |  | Length |  |
| :---: | :---: | :---: | :---: | :---: |
| Wall Deflections (Stiffness) for 1.0 kip load :  <br> Along Wall "y" Dir $1.4919 \mathrm{E}-002$ in <br> Along Wall "x" Dir $9.8787 \mathrm{E}+006$ in | Y Wall C.G. Location <br> Wall Angle CCW Wall Fixity | $\begin{gathered} 0 \mathrm{ft} \\ 0 \mathrm{deg} \\ \text { Fix-Fix } \end{gathered}$ | Height <br> Thickness <br> E-Bending <br> E - Shear | $\begin{gathered} 7 \mathrm{ft} \\ 0.5 \mathrm{in} \\ 1 \mathrm{Mpsi} \\ 1 \mathrm{Mpsi} \\ \hline \end{gathered}$ |
| Label : $\quad$ BOAT GARAGE RIGHT  <br> Wall Deflections (Stiffness) for 1.0 kip load :  <br> Along Wall "y" Dir $3.1007 \mathrm{E}-002$ in <br> Along Wall "x" Dir $1.3172 \mathrm{E}+007$ in | X Wall C.G. Location Y Wall C.G. Location Wall Angle CCW Wall Fixity | $\begin{gathered} 32.5 \mathrm{ft} \\ 0 \mathrm{ft} \\ 0 \mathrm{deg} \\ \text { Fix-Fix } \end{gathered}$ | Length <br> Height <br> Thickness <br> E - Bending <br> E - Shear | $\begin{aligned} & 3 \mathrm{ft} \\ & 7 \mathrm{ft} \\ & 0.5 \mathrm{in} \\ & 1 \mathrm{Mpsi} \\ & 1 \mathrm{Mpsi} \end{aligned}$ |
| Beam Information |  |  |  |  |
| Label : REAR MIDDLE COL | X Beam C.G. Location <br> Y Beam C.G. Location <br> Beam Angle CCW <br> Beam Fixity | $\begin{gathered} 58.25 \mathrm{ft} \\ 37 \mathrm{ft} \\ 0 \mathrm{deg} \\ \text { Fix-Fix } \end{gathered}$ | 1-xx <br> I-yy <br> E - Bending | 144 in^4 144 in^4 58 Mpsi |
| Label : REAR RIGHT COL | X Beam C.G. Location <br> Y Beam C.G. Location <br> Beam Angle CCW <br> Beam Fixity | $\begin{gathered} 71 \mathrm{ft} \\ 37 \mathrm{ft} \\ 0 \mathrm{deg} \\ \text { Fix-Pin } \end{gathered}$ | I-xx <br> I-yy <br> E - Bending | 144 in^4 144 in^4 58 Mpsi |
| Label: RIGHT FRONT COL | X Beam C.G. Location <br> Y Beam C.G. Location <br> Beam Angle CCW <br> Beam Fixity | $\begin{gathered} 71 \mathrm{ft} \\ 4 \mathrm{ft} \\ 90 \mathrm{deg} \\ \text { Fix-Fix } \end{gathered}$ | $\begin{aligned} & \text { I-xx } \\ & \text { I-yy } \\ & \text { E-Bending } \end{aligned}$ | 144 in^4 144 in $^{\wedge} 4$ 58 Mpsi |
| Label: RIGHT SECOND | X Beam C.G. Location <br> Y Beam C.G. Location <br> Beam Angle CCW <br> Beam Fixity | $\begin{gathered} 71 \mathrm{ft} \\ 25.5 \mathrm{ft} \\ 90 \mathrm{deg} \\ \text { Fix-Fix } \end{gathered}$ | $1-x x$ $1-y y$ <br> E - Bending | 144 in^4 144 in $^{\wedge} 4$ 58 Mpsi |
| Label: RIGHT THIRD | X Beam C.G. Location <br> Y Beam C.G. Location <br> Beam Angle CCW <br> Beam Fixity | $\begin{gathered} 71 \mathrm{ft} \\ 15.5 \mathrm{ft} \\ 90 \mathrm{deg} \\ \text { Fix-Fix } \end{gathered}$ | $1-x x$ 1-yy <br> E - Bending | 144 in^4 144 in $^{\wedge} 4$ 58 Mpsi |
| ANALYSIS SUMMARY | Maximum shear forces applied to resisting elements. Eccentricity with respect to Center of Rigidity |  |  |  |


| Resisting Element | Load Angle | Max Shear along Member Leral $\mathrm{y}^{\text {y }} \mathrm{y}$ " Axis |  |  |  | Max Shear along Member Local "x-x" Axis |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | X-Ecc (ft) | Y-Ecc (ft) | Shear Force (k) | Lod Angle | X-Ecc (ft) | Y-Ecc (ft) | Shear Force (k) |
| BOAT GARAGE L | 0 | -3.65 | -16.70 | 0.201 | 90 | -0.10 | -14.85 | 0.000 |
| AT GARAGE MIDD | 0 | -3.65 | -16.70 | 0.418 | 90 | -0.10 | -14.85 | 0.000 |
| JAT GARAGE RIGr | 0 | -3.65 | -16.70 | 0.201 | 20 | -0.10 | -14.85 | 0.000 |
| ARPORT VESTIBUI | 90 | -3.65 | -13.00 | 3.023 | 0 | -0.10 | -14.85 | 0.000 |
| ELEVATOR REAR | 0 | -0.10 | -14.85 | 1.637 | 90 | -0.10 | -14.85 | 0.000 |
| :RONT STAIRWELI | 0 | -3.65 | -16.70 | 0.625 | - 90 | -0.10 | -14.85 | 0.000 |
| INTERIOR FRONT | 90 | -3.65 | -13.00 \} | 1.899 | 0 | -0.10 | -14.85 | 0.000 |
| INTERIOR REAR | 90 | -3.65 | -13.00 | 0.983 | 0 | -0.10 | -14.85 | 0.000 |
| LEFT WALL | 45 | -6.72 | -15.77 | 7.923 | $\{0$ | -0.10 | -14.85 | 0.000 |
| REAR LEFT | 0 | -0.10 | -14.85 | 8.132 | 20 | -0.10 | -14.85 | 0.000 |
| zEAR MIDDLE COL | 0 | -0.10 | -14.85 | 3.143 | ) 90 | -0.10 | -14.85 | 0.000 |
| REAR RIGHT COL | 0 | -0.10 | -14.85 | 0.786 | 90 | -0.10 | -14.85 | 0.000 |
| RIGHT FRONT COL | 45 | -3.65 | -16.70 | 1.122 | 315 | -0.10 | -14.85 | 0.000 |
| RIGHT SECOND | 45 | -3.65 | -16.70 | 1.675 | 315 | -0.10 | -14.85 | 0.000 |
| RIGHT THIRD | 45 | -3.65 | -16.70 | 1.457 | 315 | -0.10 | -14.85 | 0.000 |

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Torsional Analysis of Rigid Diaphragm
. 4 JUN 2021. 10.53AM
File: DAVE COULTER.ec6
[Lic. \#: KW-06009465
DESCRIPTION: RELATIVE RIGIDITY FOR LOWER LEVEL
Layout of Resisting Elements


Torsional Analysis of Rigid Diaphragm
Project Descr:Two - Story @ 35465 Rueppell Ave

Software copyight ENERCALC, INC. 1983-2020, Buidi:12:20.5.3.
DESCRIPTION: RELATIVE RIGIDITY FOR LOWER LEVEL

## Analysis Notes

This program is designed to distribute an applied shear load to a set of resisting elements.
Each resisting element data entry specifies a deflection along a "major" and "minor" axis due to a $1,000 \mathrm{lb}$ load. Each resisting element may be entered as a wall or a column (whereby the deflection is calculated), or as a generic resisting element with specified deflection. The deflections define the stiffness of each resisting element.

Each resisting element is defined at an $(X, Y)$ location from a datum the user has previously defined. A counter-clockwise rotation of the element can be entered with respect to a traditional " +X " axis line.

A main "shear" load and an optional orthogonal shear load are specified for distribution to the system of resisting elements. In addition the maximum orthogonal dimensions of the structure and minimum accidental eccentricity percentage are specified.

From the entered loads the program calculates resultant force vectors for each angular orientation that is requested. The force is applied to the resisting elements in angular increments to generate a series of resulting direct and torsional shear loads on each element. This application of force is then repeated at angular intervals along an elliptical path defined by the minimum accidental eccentricity.

The end result is a table of direct shear and torsional shear values for each element from the iterated angles of load application and accidental eccentricity. These values are then searched to find the maximum major and minor axis shears applied to each resisting element.

|  | Project <br> COULTER SHEAR WALLS | Engineer: Phil <br> Date: $5 / 31 / 2021$ | Project \# <br> 28 PV 21 |
| :--- | :--- | :--- | :--- |
|  | Subject <br> Shearwall Design | Page |  |
|  |  |  |  |

Wall Line: FRONT WALLS AT BOAT GARAGE
Floor Level: LOWER LEVEL

## Unit Shear Calculations

Seismic Design Category D, E, or F? $\square$ yes

REFERENCE DRAWINGS FOR SHEARWALL TYPE AND SCHEDULE PLUS HOLDOWNS.
$\begin{aligned} & \text { Lateral Load to Wall Line }=820 \\ & \mathrm{lbs} \\ & \text { Total Length of Shearwalls }=10.0 \\ & \mathrm{ft}\end{aligned}$
Unit Shear Load $(v)=82$ plf

| Use Shearwall Type |  |
| :---: | :---: |
| EARTHQUAKE | W1ND |
| P1-6 | P1-6 |

Reference attached shearwall schedule for more information.

## Overturning Calculations



Seismic Controlled Design?
yes
(Affects aspect ratio)

```
Terminology: V = Panel Shear (lbs)
W = Panel Self Weight (lbs)
w = Trib. Roof/Floor Load (plf)
\(P_{d l}=D L\) Reaction from Header/Beam (lbs)
\(\mathrm{P}_{\mathrm{u}}=\) Uplift from Shearwall Above (lbs)
OTM = Overturning Moment (ft-lbs)
RM = DL Resisting Moment (ft-lbs)
Equations: \(V=v L\)
\(\mathrm{OTM}=\mathrm{VH}\)
\(R M=0.9\left[(W+w L)(L / 2)+P_{d i} L\right]\)
\(U=(O T M-R M) / L+P_{u}\)
```

Load Check, $\Sigma V=$
Max. Aspect Ratio:
Check Aspect Ratio:
(Ref. IBC Table 2305.3.3, footnote (a), when aspect ratios are exceeded)

| $\mathrm{H}(\mathrm{ft})$ | $\mathrm{L}(\mathrm{ft})$ | V | W | w | Pdl | Pu | Uplift $(\mathrm{U})$ | Req'd Holdown |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7.0 | 4.0 | 328 | 680 |  |  | 0 |  | FDN HD | FLOOR STRAP |
| 7.0 | 3.0 | 246 | 510 | 45 | 135 | 0 | 162 | NA | NA |
| 7.0 | 3.0 | 246 | 510 | 45 | 135 | 0 | 162 | NA |  |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |


|  | Project <br> COULTER SHEAR WALLS | Engineer: Phil <br> Date: $5 / 31 / 2021$ | Project \# <br> $28 P V 21$ |
| :--- | :--- | :--- | :--- |
|  | Checker: <br> Shearwall Design | Page |  |
| Date: |  |  |  |


| Wall Line: | LEFT WALL |
| :--- | :--- |
| Floor Level: | LOWER LEVEL |

## Unit Shear Calculations

Seismic Design Category D, E, or F? $\square$ yes

REFERENCE DRAWINGS FOR SHEARWALL TYPE AND SCHEDULE PLUS HOLDOWNS.
$\begin{aligned} & \text { Lateral Load to Wall Line }=8,300 \\ & \text { lbs } \\ & \text { Total Length of Shearwalls }=34.0 \mathrm{ft}\end{aligned}$

$$
\begin{aligned}
& \text { Unit Shear Load }(v)=244 \text { plf } \longleftarrow \longleftarrow \frac{\text { WIND }}{\text { P1-6 }}
\end{aligned}
$$

Reference attached shearwall schedule for more information.

## Overturning Calculations



Seismic Controlled Design? $\square$
yes (Affects aspect ratio)

Terminology: V = Panel Shear (lbs)
W = Panel Self Weight (lbs)
w = Trib. Roof/Floor Load (plf)
$\mathrm{P}_{\mathrm{dl}}=$ DL Reaction from Header/Beam (lbs)
$\mathrm{P}_{\mathrm{u}}=$ Uplift from Shearwall Above (lbs)
OTM = Overturning Moment (ft-lbs)
RM = DL Resisting Moment (ft-lbs)
Equations: $V=v L$
$\mathrm{OTM}=\mathrm{VH}$
$R M=0.9\left[(\mathrm{~W}+w L)(\mathrm{L} / 2)+\mathrm{P}_{\mathrm{di}} \mathrm{L}\right]$
$U=(O T M-R M) / L+P_{u}$

Load Check, $\Sigma V=$ 8,300 (Compare w/Load Above)
Max. Aspect Ratio:
2.0

OK
(Ref. IBC Table 2305.3.3, footnote (a), when aspect ratios are exceeded)

| $\mathrm{H}(\mathrm{ft})$ | $\mathrm{L}(\mathrm{ft})$ | V | W | w | Pdl | Pu | Uplift (U) | Req'd Holdown |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 34.0 | 8,300 | 6,800 |  |  |  |  | NA | NA |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | FLOOR STRAP |  |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |


|  | Project <br> COULTER SHEAR WALLS | Engineer: Phil <br> Date: $5 / 31 / 2021$ | Project \# <br> 28 PV21 |
| :--- | :--- | :--- | :--- |
|  | Subject <br> Shearwall Design | Page |  |
|  |  |  |  |


| Wall Line: | WALL AT ELEVATOR |
| :--- | :--- |
| Floor Level: | LOWER LEVEL |

## Unit Shear Calculations

Seismic Design Category D, E, or F? $\square$ yes

REFERENCE DRAWINGS FOR SHEARWALL TYPE AND SCHEDULE PLUS HOLDOWNS.
$\begin{aligned} \text { Lateral Load to Wall Line } & =1,637 \mathrm{lbs} \\ \text { Total Length of Shearwalls } & =7.5 \mathrm{ft}\end{aligned}$


Reference attached shearwall schedule for more information.

## Overturning Calculations



Seismic Controlled Design?
yes
(Affects aspect ratio)
Terminology: V = Panel Shear (lbs)
W = Panel Self Weight (lbs)
w = Trib. Roof/Floor Load (plf)
$P_{\mathrm{dl}}=$ DL Reaction from Header/Beam (lbs)
$\mathrm{P}_{\mathrm{u}}=$ Uplift from Shearwall Above (lbs)
OTM = Overturning Moment (ft-lbs)
RM $=$ DL Resisting Moment (ft-lbs)
Equations: $V=v L$
OTM = VH
$R M=0.9\left[(\mathrm{~W}+w \mathrm{~L})(\mathrm{L} / 2)+\mathrm{P}_{\mathrm{dl}} \mathrm{L}\right]$
$U=(O T M-R M) / L+P_{u}$

Load Check, $\Sigma V=1,637$ (Compare w/Load Above)
Max. Aspect Ratio:
2.0

Check Aspect Ratio:
OK
(Ref. IBC Table 2305.3.3, footnote (a), when aspect ratios are exceeded)

| $\mathrm{H}(\mathrm{ft})$ | $\mathrm{L}(\mathrm{ft})$ | V | W | w | Pdl | Pu | Uplift (U) | Req'd Holdown |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7.0 | 7.5 | 1,637 | 1,275 |  |  |  |  | FDN HD | FLOOR STRAP |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA |  |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |



| Wall Line: | FRONT OF VESTIBULE AT STAIRWELL |
| :--- | :--- |
| Floor Level: | LOWER LEVEL |

## Unit Shear Calculations

Seismic Design Category D, E, or F? yes

REFERENCE DRAWINGS FOR SHEARWALL TYPE AND SCHEDULE PLUS HOLDOWNS.
$\begin{aligned} & \text { Lateral Load to Wall Line }=623 \mathrm{lbs} \\ & \text { Total Length of Shearwalls }=7.5 \\ &\end{aligned}$

Use Shearwall Type
EARTHQUAKE

| P1-6 | WIND |
| :---: | :--- |
| P1-6 |  |

Reference attached shearwall schedule for more information.

## Overturning Calculations



Seismic Controlled Design?
yes (Affects aspect ratio)

Terminology: V = Panel Shear (lbs)
W = Panel Self Weight (lbs)
w = Trib. Roof/Floor Load (plf)
$P_{\mathrm{dl}}=$ DL Reaction from Header/Beam (lbs)
$\mathrm{P}_{\mathrm{u}}=$ Uplift from Shearwall Above (lbs)
OTM = Overturning Moment (ft-lbs)
RM = DL Resisting Moment (ft-lbs)
Equations: $V=v L$
OTM = VH
$R M=0.9\left[(\mathrm{~W}+\mathrm{wL})(\mathrm{L} / 2)+\mathrm{P}_{\mathrm{dl}} \mathrm{L}\right]$
$\mathrm{U}=(\mathrm{OTM}-R M) / L+\mathrm{P}_{\mathrm{u}}$

Load Check, $\Sigma V=623$ (Compare w/ Load Above)
Max. Aspect Ratio:
Check Aspect Ratio:
2.0

OK
(Ref. IBC Table 2305.3.3, footnote (a), when aspect ratios are exceeded)

| $\mathrm{H}(\mathrm{ft})$ | $\mathrm{L}(\mathrm{ft})$ | V | W | w | Pdl | Pu | Uplift (U) | Req'd Holdown |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7.5 | 623 | 1,275 |  |  |  |  | FDN HD | FLOOR STRAP |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA |  |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |
| 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 | 0 | NA | NA |



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Project Title: New Home for Pattie and Dave Coulter Engineer: S/P
Project ID: 28PV21
Project Descr: Two - Story @ 35465 Rueppell Ave

DESCRIPTION: CANTILEVERED COLUMNS - PILASTERS CONTINUE ABOVE FOUNDATION WALL


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## Code References

Calculations per ACI 318-14, IBC 2018, CBC 2019, ASCE 7-16
Load Combinations Used : IBC 2018


Column Cross Section
Column Dimensions: 12.0 in Square Column, Column Edge to
Rebar Edge Cover $=1.50$ in

Column Reinforcing : 4 - \#6 bars @ corners,



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Maximum Deflections for Load Combinations


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## Sketches




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Concrete Column P-M Interaction Diagram


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Concrete Column P-M Interaction Diagram


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Concrete Column P-M Interaction Diagram


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Concrete Column P-M Interaction Diagram



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Concrete Column
Lic. \# : KW-06009465
DESCRIPTION: CANTILEVERED COLUMNS - PILASTERS CONTINUE ABOVE FOUNDATION WALL

Concrete Column P-M Interaction Diagram


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Concrete Column P-M Interaction Diagram


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## DAVE \& PATTIE COULTER RESIDENCE DETAILS

|  | SCHEDULE |
| :--- | :--- |
| DTL-1 | EAVE \& GUTTER DETAIL |
| DTL-2 | EAVE @ RAKE DETAIL |
| DTL-3 | OVERHANG DETAIL |
| DTL-4 | DECK EDGE @ SOUTH DETAIL |
| DTL-5 | DECK @ GARAGE DOOR DETAIL |
| DTL-6 | DECK EDGE @ EAST CARPORT WALL DETAIL |
| DTL-7 | DECK EDGE @ SOUTH CARPORT DETAIL |
| DTL-8 | DECK @ OUTDOOR KITCHEN DETAIL |
| DTL-9 | DECK BEAM CONNECTION @ EXISTING HOUSE DETAIL |
| DTL-10 | COLUMN @ TIMBER FRAME PATIO COVER DETAIL |
| DTL-11 | GARAGE WALL @ FOUNDATION DETAIL |
| DTL-12 | CLIPPED EAVE DETAIL |
| DTL-13 | B-4 to B-5 \& B-18 STEEL PLATE CONNECTION DETAIL |
| DTL-14 | STEEL STAIR CONNECTION TO WALL DETAIL |
| DTL-15 | DECK STAIR @ EXISTING HOUSE DETAIL |
| DTL-16 | VERT. SIDING AT BOTTOM OF WALL w/ HORIZ. NAILER \& DRAINAGE STRIP |
| DTL-17 | VERT. SIDING AT BOTTOM OF WALL DRAINAGE STRIP DETAIL |



## EAVE AND GUTTER DETAIL

SCALE

$1-1 / 2^{\prime \prime}=1^{\prime}-0 "$


## EAVE @ RAKE DETAIL




## DECK EDGE @ SOUTH DETAIL

SCALE

$1-1 / 2^{\prime \prime}=1^{\prime}-0{ }^{\prime \prime}$


## DECK @ GARAGE DOOR DETAIL

SCREW TO TOP RAIL OF DESIGN RAIL. COUNTER SINK AND PLUG

WOOD TOP CAP w/ LED LIGHTING

## FEENY CABLE RAIL SYSTEM 2-3/8" SQUARE POST, $\longrightarrow$

 MAX SPACING 6'-0" o.c.

ATTACHMENT SCREW, (2 PER SIDE, 4 PER POST) SET END PAVER IN MASTIC STANCHION, ATTACHED TO STRUCTURE

COLOR MATCHED FLASHING 8/4 x 6 AZEK TRIM 1×4 HORIZ. AZEK CLADDING o/ WEATHER PROOFING

SHEAR WALL



## DECK EDGE @ SOUTH CARPORT DETAIL



## DECK @ OUT DOOR KITCHEN DETAIL





## COLUMN @ TIMBER FRAME PATIO COVER DETAIL



## GARAGE WALL @ FOUNDATION DETAIL

$$
\text { SCALE } \quad 3^{\prime \prime}=1^{\prime}-0^{\prime \prime}
$$



SCALE

## NOT ALL COMPONENTS ARE SHOWN FOR CLARITY



## B-4 to B-5 \& B-18 STEEL PLATE CONNECTION DETAIL

SCALE



## DECK STAIR @ EXISTING HOUSE DETAIL

# Vertical Siding At Bottom of Wall With Horizontal Nailer and Drainage Strip Detail 

Corrugated Lath Strip ${ }^{1 / 4}$ (CL5 3845 316) and Vented Edge Metal ${ }^{\text {l/m }}$ (VMEM 3168)



MTI details are created from sources deemed to be reliable. However, MTl does not guarantee the accuracy or completeness of any information, nor shall be held responsible for amy errors, omissions, or darnages arising out of the use of this information. These details are creabed with the understanding that MTl is providing information but is not attempting to render engineering or other professional service. If such services are required, the assistance of an appropriate professon should be sought. Use MTl materials in stract conformance with local building codes and regulations. Consult local code/code officials prior to installation. It is the buyer's responsibility to ensure that MTI materials are used in strict conformance with local building codes and regulations.

## Vertical Siding At Bottom of Wall Drainage Detail

Sure Cavity ${ }^{\text {In }}$ (SC 5016 or SC 5032) or Gravity Cavity ${ }^{\text {N }}$ (GC 1816 or GC 1832 ) and Vented Edge Metal ${ }^{\text {TM }}$ (VMEM 3168)


MT details are created from sources deemed to be reliable. However, MTl does not guarantee the accuracy or completeness of any information, nor shall be held responsible for a ry errors, omissions, or damages arising out of the use of this information. These details are creabed with the understanding Ehat MTl is providing information but is not attempting to render engineening or other professional service. If such services are required, the assistance of an appropriate profession should be sought. Use MII materials in strict conformance with local building codes and regulations. Consult local code/code officials prior to installation. It is the buyer's responsibility to enisure that MTI materials are used in strict conformance with local building codes and regulations.

April 29, 2021
Ronald Coulter
105 N. Emerson
P. O. Box 2323

Chelan, WA 98816
ron.coulterarchitects@gmail.com

## Re: Soil Assessment at 35465 Rueppell Ave. in the Airport area of Pacific City, Oregon Project \#21-04-Cou

Dear Mr. Coulter:
At your request, I have completed a review of the soil conditions at your property. This investigation included document research and knowledge of the area. Site inspection will be made during the excavation and additional information may be incorporated at that time.

The property is nearly flat and about one-third of an acre in size. The rear half of the property is about 3 feet lower than the front half. The property fronts Rueppell Avenue to the southwest for about 100 feet and extends about 130 feet to the northeast. The property borders the Pacific City Airport to the east for 100 feet.

According to the USDA Natural Resources Conservation Service, the soil on the site is Urban land-Udorthents complex, with a 0 to 7 percent slope. In this soil profile, silty clay loam begins at a depth of about 14 inches and continues down several feet. When firm, silty clay loam is typically acceptable for constructing a foundation, with an allowable soil bearing pressure of 1500 pounds per square foot. In order to protect the silty clay from wet weather and degradation during construction activities, a layer of crushed rock should be placed over the soil and thoroughly compacted. The crushed rock layer should be about 4 inches thick.

Since this area does flood, the soil could be weakened when saturated. In order to further improve the site and secure the foundation, excavate the soil below the footings and replace it with pit-run rock. I recommend that the rock fill be at least 2 feet deep and a minimum width of 5 feet, centered on the footing. The rock should be mechanically compacted. Cover the pitrun rock with crushed rock for constructability.

## RONALD COULTER

Inspection at 35465 Rueppell Ave.
Pacific City, OR

Drainage from the new building should be disposed of on the surface at least 10 feet away from the house, preferably to the east. Due to the topography of the area and the flat site, foundation drains are not necessary.

Please contact me if you have any questions, or if the County requires additional information.
Sincerely,
Morgan Civil Engineering, Inc.


Jason R. Morgan, PE
Professional Engineer

cc: Project File \#21-04-Cou
<V:\21-04-Cou\Reports\Coutler site evaluation.docx>

## NOTES

THIS IS A TOPOGRAPHIC MAP OF TAX LOT 4800, PARCEL 1 AND PARCEL 2 OF PARTITION PLAT 2014-14. THE PURPOSE OF THIS MAP IS TO SHOW THE OPOGRAPHY SEE MAPS P-733, PARTTON PLAT 20014-14, TLAMOOK INFORMATION SEE MAPS P-
COUNTY SURVEY RECORDS.
elevatons are based on gps observations mit an opus solution,




## COULTER ARCHITECTURE

David and Pattie Coulter House Addition
Project Performance and Product Specification

Division 1: General Requirements:

Division 2: Site Construction:

Project to be constructed per the 2018 edition of the International Residential code (IRC) and the NFPA 70, and the National electrical code designated with the l-codes and Tillamook County codes. Direct all subcontractor and suppliers to comply with the same.

See structural General Notes on drawing S-1.5
All modifications and changes shall proceed through the architect for approval.

Shop Drawing and sample submittals required:
Steel fabrication
Windows and doors and hardware
Drywells and holding tanks, propane tanks.
SIP Panels roof panels including engineering calculations.

Warmboard Sub floor, complete system.
Finished siding, and details
Other items as noted
Dry Wells, and catch basins, located on site Plan, submit details, source: H2 pre-Cast, Wenatchee. Final locations TBD.


## COULTER ARCHITECTURE

David and Pattie Coulter House Addition<br>Project Performance and Product Specification

Utilities: final locations per the drawings

Division 3: Concrete:

Division 4: Masonry
Division 5: Metals:

## See Structural General Notes:

Architectural concrete: All exterior facing walls, and exposed interior walls, as depicted on the drawings, shall have a special finish as follows: Using new form panels with aligned snap ties as shown, shall be a smooth finish without rock pockets nor any voids.

Snap ties to be plastic cone type. See enclosed.
Provide a mock-up panel 4' x 8' with anticipated seal breaker and snap tie configuration. Mock-up panel to be subsequently buried on site.

Grouts: Non Shrink Basalite or equal
Pavers: Unilock, concrete Abbostsford, concrete
N/A
Steel frames and beam connections, welding certification required, shop drawings required, see Structural General Notes, Shop Prime

Steel tubes are HSS type steel.
Exposed Fabricated steel to be Powder Coated and non-exposed, shop primed.

Color to be selected and submitted with shops.
Steel Stair: submit shop drawing for review and approval, construct so that it can be hot dip


## COULTER ARCHITECTURE

David and Pattie Coulter House Addition
Project Performance and Product Specification
galvanized. Provide attachment as located on the drawings (with stand off through the siding rain screen, and provide footings located per the shop drawings, and sized as shown on the drawings.

Division 6: Wood and Plastics:

Exterior wall sheathing: $1 / 2$ "" CDX ( Exposure 1 rated) (most places nailed as shear walls, see shear wall diagrams.)

Dimensional beams and lumber are D.F, \#1 or better, Glue lams are framing dimensional 24/V8 unless stated otherwise. Interior Glue Lams are architectural grade.

Sub Floor: 1 1/8" Plywood WarmBoard-S on upper floor, installed per the manufactures instruction, shop drawings and required. Finish floors over WarmBoard-S to be installed per instruction manual, Installation over Joists.

Contact: Shane Banks: 206.276.376 sbanks@warmboard.com

Sill Seal at all concrete plates, and SIP Panels with Owens corning, foam seal R.

Fasteners: Sub-floor screws Simpson, Strong drive, WSV, see cut sheet, $23 / 4$ " screws.

Wood to steel: Simpson TB screws per table enclosed.


COULTER ARCHITECTURE
David and Pattie Coulter House Addition
Project Performance and Product Specification
SIP Panels by Insulspan, installation per Factory shop drawings, contractor/ installer to check shop drawing for detail and dimensional fit. See Insulspan construction manual.

Seal all joints on the warm side with factory tape See Structural notes on the drawings for perimeter nailing. Provide continuous V.B on warm side under the furring.

Contact: Dave Stevenson, 604.523.3762, cell 778.846.9512

Siding: Azek or approved equal. Vertical application with "hidden attachments" ( screws ) using the 2.5 cortex color matched plugs.

Siding mounted on horizontal nailer and drainage strip (corrugated Lath Strip ( CLS 3845-316) by MTI and vented edge metal ( VMEM 3168 wrapped with Polypropylene fabric bug screen.

Division 7: Thermal and Moisture:
Poly Wall Liquid Wrap 2300, or 2400 roll on
60 mil. Min thickness.
Joint filler 2200 with closed cell backer rod
2100 for windows and doors

STEP ONE, PREPARE AND CLEAN: (View factory video prior to application)
A. Using a stiff brush, followed by damp rag, and wipe away debris, sawdust, dirt


COULTER ARCHITECTURE
David and Pattie Coulter House Addition
Project Performance and Product Specification
or foreign matter of all surfaces including the rough opening and 6 inches around the outside perimeter of the window opening on the sheathing itself. Please note that if the substrate is wet, no problem ... Poly Wall Blue Barrier Liquid Flashing 2100 loves water.
B. Provide positive slope on the rough opening sill per Window Manufacturer's Installation Specifications. IMPORTANT: If you choose to do this you must account in advance for the space in the rough opening you take up with the positive slope or your window will not fit.

## STEP TWO, DETAIL ANY VOID UP TO 3/4" :

A. Apply PW BB 2200 Joint Filler with a plastic trowel or putty knife to holes, cracks, imperfections in rough opening \& sheathing surrounding opening.
B. In the corners, feel free to use your index finger with a damp cloth over it to press product completely into corner and smooth.
C. On average after 30 minutes product is ready for the next step depending on Relative Humidity and Temperature. If it doesn't stick to your finger upon touch it's ready.

STEP THREE: APPLY BB 2100 TO ROUGH OPENINGS:


COULTER ARCHITECTURE
David and Pattie Coulter House Addition
Project Performance and Product Specification
A. Starting on the top inside of the rough opening apply BB 2100 with sausage gun and trowel smooth so wood is not visible. Minimum 35 mils wet continuous film (46 SF / Gal coverage rate)
B. Apply in 6 -inch to 12 -inch lengths, complete inside of rough opening.
C. Apply to outside of rough opening on sheathing, approx 6 -inches wide.
D. Allow approximately 30 minutes for the flashing to set up depending on Relative Humidity and Temperature. It might still be "tacky" but as long as product does not attach to your finger at touch then your ready to install your window. STEP FOUR, INSTALL WINDOWS AND DOORS:
A. Install your window or door per manufacturer's specifications and instructions.
B. Many manufacturers call for a compatible sealant to be applied prior to the window being installed into the opening. Poly Wall Blue Barrier 2200 Joint Filler can be used for this purpose.
C. After window has been installed as directed by manufacturer specifications apply Poly Wall Blue Barrier Liquid Flashing 2100 over header and jamb flanges of the window itself with gun and trowel tying it into the existing cured fluid membrane that you had applied earlier. Make sure to completely cover the flange with fluid applied product.


## COULTER ARCHITECTURE

David and Pattie Coulter House Addition
Project Performance and Product Specification
D. It is important to leave the sill flange on the window at the bottom un-flashed with fluid flashing to allow moisture relief in the event of a window leakage.

Wet Set Installation of the rain screen hat channels: Recoat everywhere a penetration of the water barrier occurs with Blue Barrier Joint Filler 2200 when installing the hat channels that hold the Corten siding. This applies to any penetration.

Note: This project shall meet the Blower test. Review manufacturers Video before doing the work. Follow the manufactures recommendations on all steps.

Alternate W.B. Henry Blueskin VP 100, self adhered Water resistive Barrier. Install per the manufactures requirements, including moisture content and raining conditions requirements.

Rain Screen components:
Furring: Masonry Technology, Inc. Vent Edge metal (VMEM 3168), Corrugated Lath Strip (CLS 3845-316), Wrap bottom Lath Strip with Polypropylene Fabric.

Alternate: Advanced Building products, Inc. , Watairvent furr strip and Watairvent starter strip.

Roofing: Taylor Metal products, 24 Ga . Cool Kynar 500, color to be determined. Limit penetrations of the metal roof to plumbing vents, and fireplace flue, all other openings, including fans and dryer vent with INOVATE DryerJack, and Inovate Dryer Box through the walls.

Roof: Roof temporary protection during construction: GAF Deck Armor, during


## COULTER ARCHITECTURE

David and Pattie Coulter House Addition
Project Performance and Product Specification
construction, with Ice Guard at the perimeter 4 feet wide.

Final roof deck membrane: Under the metal roof, apply 11 mm VaproShield, Warp Shield RS rain screen.

Vapor Barrier ( class 1 ) required on warm side of all SIP panels, Factory supplied tape to all joints.

Insulation:
Floors: R-30 Rock Wool between the garage and upper floor.

Walls: Closed cell foam, Foamular NGX, in all walls, seal all wall to roof intersection and floor intersections, all corners air tight, 6"=wall R-33, 8"= wall-R-37.5

SIP panels, 12" -R-59.1, Factory applied. High performance GPS Insulation. Factory tape all joints. Apply vapor barrier on entire warm side.

Division 8: Doors \& Windows:
Windows and exterior doors: Loewen windows and doors except as shown.

The south facing glass, windows A \& B on the schedule, to be design to resist 125 MPH wind loading.

Shop drawings and color samples required

[^1]

## COULTER ARCHITECTURE

David and Pattie Coulter House Addition

## Project Performance and Product Specification

Division 9: Finishes:

Division 10: Specialties:

Interior details and cabinets to follow.
Floors: $3 / 4$ " hardwood, acclimated and stained all sides, all rooms except the shower and $1 / 2$ bath.

Alternate floor: Pre-finished hardwood engineered floor system, submit specs.

Ceilings in the great room, master bedroom, bathroom, and entry are 5/8" T\& G \# 1 D.F. with recess at the perimeter for LED cont. lighting strips. Exterior soffits to match.

IPE Exterior handrail: finish with Messmwe's U.V. Plus, with LED cont. lighting.

Gacodeck: All exterior deck and stair walking surface to be covered with Gacodeck, an Acrylic Polymer blend not to be installed over more than an $18 \%$ moisture content.

Use Gacodeck Polyester Reinforcing tape on the stair nosing and terminations

Gacodeck Priner to be utilized in cold weather applications.

Gacodeck Granules to be used on the waling surfaces.

Color: Standard Oyster, or to match concrete pavers as close as possible. A special color may be needed, and as approved by the Architect.

Fireplace: Flare fireplaces, see plan, submit shop R.I. dwgs, Flue to exit SIP Panels, submit detail.


## COULTER ARCHITECTURE

David and Pattie Coulter House Addition
Project Performance and Product Specification
Toilet and Bath accessories TBD
Handicap Bars: provide backing, and see interior elevations.

Shower doors: frameless glass. Submit shop drawings.

Handrails:
Cable railings- Keuka Studios, powder coated, $42^{\prime \prime}$ mounted off set with powder coated sleeves as shown on the details.

Screens by US Centor S2 double screen, 102 $3 / 8^{\prime \prime} \times 124^{\prime \prime}$, layout to be determined.

Division 11: Equipment:

Division 12: furnishings:
Division 13: Special Construction:

Security systems TBD
Appliances: supplied by the owner, installed by the contractor.

N/A
Roof structure: SIP Panels are Insulspan, with Graphite Polystyrene cores (GPS) 12" plumb cut (R59.1 @ 25 deg F.) Shop Dwgs. and Engineers stamp required. Limit penetrations to plumbing only and fireplace, all other penetrations to be side wall, utilizing dryer vents and grills by Seiho SB-P, and JSP grilles.

Warmboard on main floor 11/8" Plywood, with a sealer (glued and screwed.) Installation.
Shop installation drawings required.


## COULTER ARCHITECTURE

David and Pattie Coulter House Addition
Project Performance and Product Specification
Division 14: Conveying Systems: Elevator by: Symmetry Elevator Solutions, (or approved equal) inline gear drive at the top. See specification cut sheet.

Car size $40 \times 54$, accordion door, same side opening.

All electronics to be installed above elevation $17^{\prime}$ and the car to be set to wait at the upper level.

Division 15: Mechanical:

Division 16: electrical:
Water heater: 150 Gal. heat pump configuration.
HVAC, Mini-Split, (no duct work) design build by Sub-Contractor and collaboration with Architect.

Mitsubishi or approved equal.
Room units Located on the fireplace wall in recessed openings on the fireplace wall, see plan.

Electrical floor pians- Preliminary layout Dwgs. E-1.1 and E-1.2

Lutron square Trim: typical, color to be selected.
Ceiling Fans: Big Ass Fan, 6' dia. Remote controls

Special outlets: Locate in the field, Kitchen counter: Mockett pop up in counter and bar.

Walk through with the subcontractor required prior to installation.


COULTER ARCHITECTURE
David and Pattie Coulter House Addition
Project Performance and Product Specification

| Bath Room Heated floors: | Master Bath shower: The heated floor system to <br> be Schluter Ditra-Heat-Duo system, install per the <br> manufacturer, with controls. See plan for area. |
| :--- | :--- |
| Miscellaneous: | Glass: Discuss with the owner, Electrochromic <br> adjustable performance glass, and bird strike <br> technology prior to ordering glass, <br> guardianglass.com, Bird1st |
| Window shades: | J-Geiger, R series, with $21 / 2 "$ dia. Jamb brackets, <br> clear anodized. Black out fabric for the master <br> suites, and Translucent for the living room and <br> dining Room, remote controlled, wired in motors, <br> coordinated with Lutron, see Electrical. |
| Patio gas fired tables: | Paloform or approved equal |

[^2]Hot limb deck floor drain
$60^{\prime \prime}$

## - Linear Shower Drain - Pattern Grate

P.O. Box 8064, Atlanta, GA 31106 p: 877.398.8110 f. 877.388.1239
e: sales@lineardrains.com www.lineardrains.com

Channel for Easy Cleaning


Section $A-A^{\prime}$
Standard Linear Drain Lengths



## MODEL ZB110 VENTILATION FAN



## FEATURES

## UltraGreen ${ }^{\text {TM }}$ Energy Saving DC Motor

- DC motor for efficiency well beyond ENERGY STAR ${ }^{\text {® }}$ requirements.
- Multi-speed capability ideal for meeting ASHRAE 62.2, LEED and ENERGY STAR ${ }^{\oplus}$ for Homes requirements. Can be used to comply with CA Title 24, as well as local/spot ventilation needs.


## UltraSilent ${ }^{\text {TM }}$ S ound Technology

- HVI certified, best-achievable <0.3 Sone level provides nearly silent operation for a relaxing environment.
- State-of-the-art blower and duct outlet design smooths airflow.
- High tech DC motor designed for nearly silent operation.

UltraSmart ${ }^{\text {TM }}$ C ontrol Technology

- Powerful operation maintained over a wide range of real-world installations (CFM ratings maintained through at least $0.25^{\prime \prime}$ static pressure).
- Infinitely adjustable low cfm setting allows precise adjustment to prevent over-ventilating and maximize efficiency.
- Adjustable time delay sets how long fan will run on high speed before returning to a continuous lower speed.


## UltraQuick ${ }^{\text {TM }}$ Installation Technology

- Unique telescoping mounting frame fits through retrofit drywall opening to allow easy installation from the room side. No attic access needed!
- Captive screws allow for easy new construction installation.
- Mounting frame positioning tabs provide easy vertical positioning for new construction.
- Easy to insert and remove snap-in housing. No screws required!
- Easy to insert and remove snap-in blower.
- Inside or outside duct connector and knockout plate mounting provides flexibility for new construction or retrofit.
U.L. Listed for use over bathtubs and showers when connected to a GFCI protected branch circuit (ceiling mount only).

3-year warranty.

## DIMENSIONS (Inches)



ENERGY STAR

Broan-NuTone LLC Hartford, Wisconsin www.broan.com 800-558-1711

| REFERENCE | QTY. | REMARKS | Project |
| :--- | :--- | :--- | :--- |
|  |  |  | Location |
|  |  | Architect |  |
|  |  | Engineer |  |
|  |  | Contractor |  |
|  |  | Submitted by | Date |

HVI PERFORMANCE

| Airflow <br> Rate <br> Setting <br> (CFM) | $6^{\prime \prime}$ Duct |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Airflow <br> (CFM) | Sound <br> (Sones) | Power <br> (Watts) | Efficacy <br> (CFM/ <br> Watt) | Airflow <br> (CFM) |
|  | 110 | $<0.3$ | 7.7 | 14.2 | 110 |
| 100 | 100 | $<0.3$ | 7.0 | 14.2 | 100 |
| 90 | 90 | $<0.3$ | 6.4 | 14.0 | 90 |
| 80 | 80 | $<0.3$ | 5.8 | 13.7 | 80 |
| 70 | 70 | $<0.3$ | 5.1 | 13.7 | 70 |
| 60 | 60 | $<0.3$ | 4.6 | 13.0 | 60 |
| 50 | 50 | $<0.3$ | 4.1 | 12.1 | 50 |
| 40 | 40 | $<0.3$ | 3.7 | 10.8 | 40 |
| 30 | 30 | $<0.3$ | 3.3 | 9.0 | 30 |



HVI-2100
CERTIFIED
RATINGS comply with new testing technologies and procedures prescribed by the Home Ventilating Institute, for off-the-shelf products, as they are available to consumers. Product performance is rated at 0.1 in. static pressure, based on tests conducted in a state-of-the-art test laboratory. Sones are a measure of humanly-perceived loudness, based on laboratory measurements.

## ELECTRICAL \& WEIGHT

| Volts | Hz | Amps | Shipping <br> Weight <br> (lbs.) |
| :---: | :---: | :---: | :---: |
| 120 | 60 | 0.2 | 12.3 |

## FAN CAPABILITY



## Ultra-thin LED Recessed Light

- Uses $90 \%$ less wattage compared to comparable traditional lights


LED driver (non-dimmable)

- Easy to install: LED light fixture and LED driver (included) are all detachable.
- Very small, low profile design; its height is less than $3 / 4$ inch.
- Sturdy aluminum housing.
- High quality diffuser achieves even and soft light output.
- Incredibly bright, this High Power LED Recess Light is the perfect way to modernize your home or business by saving loads of money on your energy and maintenance costs.

Specifications

| Wattage | 12.5 Watt Max. <br> (LED fixture: approx. 9 Watt, LED driver: approx. 3.5 Watt) |
| :---: | :---: |
| LED Chip | High-Power LED (24 LEDs) |
| LED forward Current | 700 mA |
| Beam Angle | Approx. $110^{\circ}$ |
| Light Color | Warm White (approx. 3000K), Neutral White (approx. 4200K), Cool White (approx. 6000K) |
| Light Output | Warm White: 560 Im , Neutral White: 6001m, Cool White: 620 Im |
| Color Rendering Index | Cool white: $\mathrm{Ra}>70$, Warm white: $\mathrm{Ra}>75$ |
| Life Span | 50,000 hours |
| Voltage | LED driver: 100~240VAC (UL rated) |
| Dimensions | LED light fixture: <br> height: $1.3 \mathrm{~cm}\left(0.52^{\prime \prime}\right)$, diameter: 16.2 cm ( $6.38^{\text {" }}$ ) <br> LED driver (default, non-dimmable): <br> L: $65 \mathrm{~mm}\left(2.6^{\prime \prime}\right) \times \mathrm{W}: 35 \mathrm{~mm}\left(1.4^{\prime \prime}\right) \times \mathrm{H}: 23 \mathrm{~mm}\left(0.9^{\prime \prime}\right)$ |
| Casing Color | Painted white |
| Housing | LED light body: Aluminum, Cover: PMML plastic diffuser |
| Protection Rating | CE, RoHS |
| Operating Temperature | $-10^{\circ} \mathrm{C} \sim+40^{\circ} \mathrm{C}$ |

Installation Diagram


## LED Channel Strip

## DIMENSIONS


$\left(\sum_{L \text { tste }}^{0}\right)_{0}$

## APPLICATION

The LCS family of LED strip lights combine high-performance LEDs, highlyengineered optics to traditional designs to bring you the most advanced line of LED Strip Lights on the market. Multiple lumen packages mean there is an LCS that is just right for your lighting needs.

FEATURES

- Available in $2^{\prime}, 4^{\prime}$, or $8^{\prime}$ lengths
- Optional integral emergency battery pack
- Surface mount or suspended
- Heavy die-formed steel channel
- All luminaires are built to UL 1598 and 2108 standards, and bear appropriate ETL labels


## FEATURES \& SPECIFICATIONS

INTENDED USE - LBL LED wraparound provides a digital lighting platform to deliver general ambient lighting for surface-mount applications. The LED system delivers long life and excellent color to ensure a quality, low-maintenance lighting installation. Ideal for closets, storage rooms, hallways, and offices.
CONSTRUCTION — Metal parts are die formed from code-gaugesteel. Prismatic diffuser is $100 \%$ acrylic with sonically welded luminous ends. Continuous side flanges on fixture body provide light trap and continuous diffuser support to prevent accidental opening and simplify maintenance.
Finish: Five-stage iron phosphate pretreatment assures superior paint adhesion and rust resistance. Painted parts finished with high-gloss, high-reflectivity baked white polyester enamel (low VOC).
OPTICS - Curved prismatic diffuser with linear side prisms and highly transmissive overlay minimizes lamp image and provides high-angle brightness control. Luminous end plates soften appearance for improved aesthetics.

ELECTRICAL - Long-lifeLEDs, coupled with high-efficiencydrivers, provide extended servicelife. $90 \%$ LED lumen maintenance at 60,000 hours ( $\mathrm{L} 90 / 60,000$ ).
LED drivers deliver dimming from 0-10V control signal.
LISTINGS - CSA certified to U.S. and Canadian standards. Damplisted.
DesignLights Consortium ${ }^{\circ}$ (DLC) qualified product. Not all versions of this product may be DLC qualified. Please check the DLC Qualified Products List at www.designlights.org/OPL to confirm which versions are qualified.
WARRANTY - 5 -year limited warranty. Complete warranty terms located at www.acuitybrands.com/CustomerResources/Terms and conditions.aspx
Note: Actual performance may differ as a result of end-user environment and application.
All values are design or typical values, measured under laboratory conditions at $25^{\circ} \mathrm{C}$.
Specifications subject to change without notice.


All dimensions are inches (centimeters) unless otherwise indicated.

| Catalog <br> Number |
| :--- |
| Notes |
| Type |

## Contractor Select

 LBLED
# Low-Profile Curved-Basket LED Wraparound 



## MOUNTING DATA

Individual Installation -
Two single-stem hangers required.
Row Installation -
One hanger per fixture plus one row required.


OBDERINGINFORMAIION
See LBL Configurable specification sheet for additional lumen packages and control options.

| Catalog number | UPC | Description | Lumens | Color temperature | Lens type | Voltage | Wattage ${ }^{2}$ | Pallet qty | Standard carton पty. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LBL2 LP835 ${ }^{\text {a }}$ | 753573917564 | 2'LED Wraparound | 2,248 | 3500 K | Patterned \#12 acrylic | 120-277 | 23 | 112 | 1 |
| LBL2 LP840' | 753573917595 | 2'LED Wraparound | 2,267 | 4000 K | Patterned \#12 acrylic | 120-277 | 23 | 112 | 1 |
| LBL4LP835 | 753573917601 | $4^{\prime}$ ED Wraparound | 4,564 | 3500 K | Patterned 12 acylic | 120-277 | 41 | 56 | 1 |
| LBL4LP840 ${ }^{\text {a }}$ | 753573917632 | 4'ED Wraparound | 4,600 | 4000 K | Patterned\# 12 acrylic | 120-27 | 41 | 56 | 1 |
| LBL4 347 LP835 | 753573917649 | 4'LEDWraparound | 4,564 | 3500 K | Patterned\#12 acrylic | 347 | 41 | 56 | 1 |
| LBL4 347 LP840 | 820476010279 | 4' LED Wraparound | 4,600 | 4000 K | Patterned \#12 acrylic | 347 | 41 | 56 | 1 |

## LBL Low Profile LED Wraparound

## PHOTOMETRICS

LBL2 LP840, 2266.8 delivered lumens, test no. LTL27384P5, tested in accordance to IESNA LM-79.


| pfpc | Coefficients of Utilization |  |  |
| :---: | :---: | :---: | :---: |
|  | 20\% |  |  |
|  | 80\% | 70\% | 50\% |
| pw | 70\%50\%30\% | 50\%30\%10\% | 50\%30\%10\% |
| 0 | 116116116 | 112112112 | 105105105 |
| 1 | 10610298 | 999592 | $\begin{array}{llll}92 & 89 & 87\end{array}$ |
| 2 | $98 \quad 9084$ | 878176 | 827773 |
| 3 | $\begin{array}{llll}90 & 80 & 72\end{array}$ | $\begin{array}{ll}78 & 71\end{array} 65$ | $\begin{array}{ll}73 & 67\end{array} 63$ |
| ${ }^{4}$ | 837264 | $70 \quad 6256$ | $66 \quad 5954$ |
| U | $\begin{array}{ll}77 & 65\end{array} 56$ | $\begin{array}{llll}63 & 5549\end{array}$ | $60 \quad 53 \quad 48$ |
| 6 | 715950 | $\begin{array}{llll}57 & 49 & 44\end{array}$ | $54 \quad 4742$ |
| 7 | $66 \quad 54 \quad 45$ | $52 \quad 45 \quad 39$ | $\begin{array}{lll}50 & 43 & 38\end{array}$ |
| 8 | 624941 | $48 \quad 4035$ | $\begin{array}{llll}46 & 39 & 34\end{array}$ |
| 9 | $\begin{array}{llll}58 & 45 & 38\end{array}$ | $\begin{array}{llll}44 & 37 & 32\end{array}$ | $42 \quad 36$ |
| 10 | $54 \quad 4234$ | 413429 | $\begin{array}{llll}39 & 33 & 29\end{array}$ |


| Zonal Lumen Summary |  |  |  |
| :--- | :---: | :---: | :---: |
| Zone | Lumens | \% Lamp | \% Fixture |
| $0^{\circ}-30^{\circ}$ | 692 | 30.5 | 30.5 |
| $0^{\circ}-40^{\circ}$ | 1082 | 47.7 | 47.7 |
| $0^{\circ}-60^{\circ}$ | 1669 | 73.6 | 73.6 |
| $0^{\circ}-90^{\circ}$ | 2010 | 88.7 | 88.7 |
| $90^{\circ}-120^{\circ}$ | 124 | 5.5 | 5.5 |
| $90^{\circ}-130^{\circ}$ | 162 | 7.1 | 7.1 |
| $90^{\circ}-150^{\circ}$ | 225 | 9.9 | 9.9 |
| $90^{\circ}-180^{\circ}$ | 257 | 11.3 | 11.3 |
| $0^{\circ}-180^{\circ}$ | 2267 | 100.0 | 100.0 |

LBL4 LP840, 4600.4 delivered lumens, test no. LTL27386P25, tested in accordance to IESNA LM-79.



TM870LA


Our complete line of $\mathrm{P} \& S$ Decorator devices combine today's design aesthetics with ease of installation, reliability and performance that never goes out of style.

## features \& benefits

- Designer-style, satin-finish rocker style.
- High-impact resistance thermoplastic construction.
- Narrow back body leaves more room for wires in the box.
- Extra-long, through-body strap eliminates floating installations and imperfect applications.
- For covering patents, see www.legrand.us/patents.


## specifications

## General Info

Color: Light Almond
Product Series: TradeMaster
Number Of Poles: 1
Style: Decorator

## Listing Agencies/Third Party Information

CSA Listing Info: C22.2 111
CSA Standard: Yes
UL Listing No: UL20
UL Standard: Yes
UN SPS C: 39121704

## Dimensions



## 885TRLA

Decorator Tamper-Resistant Receptacle. 15 amp, 125 volt, Light Almond.


## features \& benefits

- Meets 2008 National Electrical Code Tamper-Resistant requirements.
- Protects children: patented shutter system-now with black "invisi-shutters" that disappear for an invisible effect-helps prevent improper insertion of foreign objects.
- High-impact resistant thermoplastic construction.
- Extra-long strap.
- Quickloop wire looping aid
- Long-term blade retention.
- Longer tri-drive screws for easier 12 AWG looping.
- Extra-large circuit break-off tabs.
- Side-access push wire release.
- Ultrasonic welding of face to back body.
- Side wire accepts \#12 - \#14 AWG solid wire.
- Push wire accepts \#14 AWG solid only.
- Superior protection than traditional outlet caps or protection plates.
- Low profile face.
- Traditional contoured face (3232 models).
- Self-grounding models provide automatic ground clip.
- For covering patents, see www. legrand.us/patents.


## specifications

## General Info

Color: Light Almond
Type: Tamper-Resistant


SWP26LA

Uniquely constructed P\&S Screwless Wall Plates have a no-dirt catching channel around the perimeter, ensuring a clean, uniform look.

## features \& bencitis

- Unbreakable, flexible polycarbonate construction conforms to uneven drywall.
- Smooth, sleek look hides the screws and highlights the style.
- Automatic alignment pins ensure wall plate fits perfectly.
- Smooth perimeter eliminates channel that can catch dirt.
- Includes two-piece, non-conductive polycarbonate subplate to help speed installation.


SWP262LA

Uniquely constructed P\&S Screwless Wall Plates have a no-dirt catching channel around the perimeter, ensuring a clean, uniform look.

## callies is ochellis

- Unbreakable, flexible polycarbonate construction conforms to uneven drywall.
- Smooth, sleek look hides the screws and highlights the style.
- Automatic alignment pins ensure wall plate fits perfectly.
- Smooth perimeter eliminates channel that can catch dirt.
- Includes two-piece, non-conductive polycarbonate subplate to help speed installation.


## specifications

## General Info

Color: Light Almond
Special Features: Screwless
Style: Decorator

## Listing Agencies/Third Party Information

Federal Spec: No
UN SPS C: 39121704

## Dimensions

Height U S: 4.87"
Width U S: 4.912"

Technical Information


SWP263LA

Uniquely constructed P\&S Screwless Wall Plates have a no-dirt catching channel around the perimeter, ensuring a clean, uniform look.

## features \& benetis

- Unbreakable, flexible polycarbonate construction conforms to uneven drywall.
- Smooth, sleek look hides the screws and highlights the style.
- Automatic alignment pins ensure wall plate fits perfectly.
- Smooth perimeter eliminates channel that can catch dirt.
- Includes two-piece, non-conductive polycarbonate subplate to help speed installation.


## specifications

## General Info

Color: Light Almond
Special Features: Screwless
Style: Decorator
Listing Agencies/Third Party Information
UN SPS C: 39121704

## Dimensions

Height U S: 4.87"
Width U S: 6.724"

Technical Information

Elevator Drive Systems


Winding Drum Drive System

## General

- Overhead minimum of 7'10" [94 inches) with a $7^{\prime} 0$ " interior car height


## Mechanical Equipment

- 208/230 VAC, 60HZ, 30 amp , singlephase power supply for motor controller
- Two $3 / 8$ " $7 \times 19$ galvanized aircraft cable [ 14400 lbs . breaking strength]
- Inverter-controlled variable speed winding drum drive unit and 3 hp motor
- Manual lowering device


## Safety Features

- Slack rope safety device
- Two upper and one lower final limits

Typical Hoistway Options
All hoistway dimensions reference interior dimensions-finished wall to finished wall.

Single Opening
Rail Left, Right-Hand Door (shown)
Rail Right, Left-Hand Door (opposite)


| Car Gatel Door | Car Size | Widh | Depth | Rail C/L | Door C/L | Clear Opening |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Accordion or Collapsible [2] | 36x48 | 501/2" | 541/4" | 271/2" | 283/4" | 331⁄2" |
|  | $36 \times 60$ | $501 / 2^{\prime \prime}$ | 661/4" | 331/2" | 283/4" | 331/2" |
|  | $40 \times 54$ | 541/2" | 601/4" | $32^{\prime \prime}$ | 323/4" | 331/2" 3 (3) |
| Symmetry Safety 3-Panel | 36×48 | 52" | 55" | 31" | 301/4" | 33" |
|  | $36 \times 60$ | 52" | $67^{\prime \prime}$ | $331 / 2^{\prime \prime}$ | 301/4" | 33" |
|  | 40×54 | 541/2" | 67 " | 31" | 323/4" | 33" 3 ) |

Opposite Opening
Rail Right, Left-Hand Door, Right-Hand Door
Rail Left, Right-Hand Door, Left-Hand Door


| Car Gatel Door | Car Size | Width | Depth | Rail C/L | Door C/L | Clear Opening |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Accordion or Collapsible [2] | 36x48 | 501/2" | 54" | $27^{\prime \prime}$ | 283/4" | 331⁄2" |
|  | 36x60 | 501/2" | 66" | 33" | 283/4" | 331/2" |
|  | $40 \times 54$ | 541/2" | 60" | 30" | 323/4" | 331/2" 3 (3) |
| Symmetry Safety 3-Panel | 36×54 | 52 | 61 | 31" | 301/4" | $33^{\prime \prime}$ |
|  | 36x60 | 52" | 673/4" | 34" | 301/4" | 33 |
|  | 40×54 | 541/2" | 613/4" | 31" | 323/4" | 33" 3 ] |

(1) Inline Gear Drive motor extends into the access hatch
(2) Collapsible gates will have a clear opening approximately 7 " less than shown
(3) $36^{\prime \prime}$ clear opening available-door centerlines may change

Doon centerines apply to $30^{\circ}$ " doors. excepl where otherwise noted.


## SMART VENT

## Product Catalog

Geto Pratuct Caialos
Certification
0 Downioarour Nationos


Check out our FAQs

Still Have a
Question?
Contact our Sales and Suppor! Office
( 877 ) 441-8368

- minasmaryentsom




## About Dual Function Vents

## Application

These vents are used for a home with a crawispace or any enclosed area that desires natural aif ventilation and frod protection

## Flood Protection

The vent door is latched closed untit themes m contact with flood water. Entermg flood water hitts the patented internal foats which unfatch and allow the door to rotate open. This allows the flood water to automaticaliy enfer and exit through the frome openng. reteving the pressure from the foundation walis Certifed flood debris clearame is demonstrated with a $3^{3}$ diameter opening when the flood door is activatod

## Ventilation

A bimetal con automatically opens ard closes the ventilation louvers as temperature changes No electricity is required The louvers with be fully closed at $35 F$ and fully open at 75 F . In the event of a flood the internal floats lift to selease the flood door to rotate open and relieve the hydrostatic pressure regardless of the louvers' position, open or closed

## Flood Resistant Materials

The Smant Vent product fre is consinucted out of Marine Grado Stanless Steel and is $100 \%$ made in the United States. T316L Stainless Steel is renowned for its ability to withstand usage in harsh marine and chemical enviromments, ensurng that cur products will handle everything Mother Nature throws at them Because T315L Staintess Steel is known for its strengh and resistance to cracking, dents, and embotienment if sutized in high proffe profects meant to last decades. Alloyed whth Chrome Nickel and Molybdenum, T316L Stanless Sleel takes the shength of steel and adds protection making it the tilmate fiood resistant matenal






## MINIMUM CAVITY HEIGHT PLAN VIEW



GENERAL NOTES: APPLY TO ALL OF THE ABOVE PRODUCTS

1. INSTALLATION MUST BE COMPLETED IN ACCORDANCE WITH BISON INNOVATIVE PRODUCTS SPECIFICATIONS.
2. DRAWINGS NOT TO SCALE.
3. CONTRACTOR'S NOTE: FOR PRODUCT AND COMPANY INFORMATION VISIT www.BisonIP.com
4. ADHERE- INSTALLER MUST ADHERE WITH POLYURETHANE CONSTRUCTION ADHESIVE

F LOW CAVITY HEIGHT PLACEMENT
CAVITY HEIGHTS BELOW $1 / 4^{\prime \prime}$


| Level.it / ACCESSORIES | model number | RANGE OF ADJUSTMENT | ADDS | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: |
|  | LC | 2"-43/4" | - | ADJUSTABLE PEDESTAL |
| 近 1 | C1 | $1 / 4^{\prime \prime}-11 / 2^{\prime \prime}$ | UP TO 1 1/2" | 1" COUPLER |
| $\frac{\pi}{\pi} \\|$ | C4 | $21 / 2^{\prime \prime}-4{ }^{\prime \prime}$ | UP TO 4" | 4" COUPLER |
| (88) | VT18 VT316 |  |  | $\begin{aligned} & \text { 1/8" TABS } \\ & 3 / 16^{\prime \prime} \text { TABS } \end{aligned}$ |
| 为 | HD25 | $=$ | ADDS 1/4" | FIXED HEIGHT |
| ก00 | HD50 | = | ADDS 1/2" | FIXED HEIGHT |
| 4-0.505 | HD75 | - | ADDS 3/4" | FIXED HEIGHT |
|  | LO | $11 / 4^{\prime \prime}-2^{\prime \prime}$ | $=$ | ADJUSTABLE PEDESTAL |
| $\longrightarrow$ | LD4 | $1 / 4^{\prime \prime}$ PER FOOT | ADDS 3/8" | BASE LEVELER DISK |
| $8$ | B11 | = | ADDS 1/16" | FLEXIBLE SHIM SOUND DAMPENING |
|  | PS1 | - | ADDS 1/8" | RIGID SHIM |
|  | FFB | $=$ | ADDS 1/4" | FLOATING FOUNDATION BASE $12^{\prime \prime} \times 12^{\prime \prime} \times 1 / 4^{\prime \prime}$ |
|  | FIB | = | ADDS 11/16" | FLOATING INSULATION BASE 12 " $\times 12^{\prime \prime} \times 11 / 16^{\prime \prime}$ |

GENERAL NOTES: APPLY TO ALL OF THE ABOVE PRODUCTS

1. INSTALLATION MUST BE COMPLETED IN ACCORDANCE WITH BISON INNOVATIVE PRODUCTS SPECIFICATIONS.
2. DRAWINGS NOT TO SCALE.
3. CONTRACTOR'S NOTE: FOR PRODUCT AND COMPANY INFORMATION VISIT www.BisonIP.com

LEVEL.IT PEDESTALS
PRODUCT LINE



VT316 / VT18 FIXED HEIGHT 1/8"


HD75
FIXED HEIGHT 3/4"


LC $+\mathbf{C 1}$
$43 / 4^{\prime \prime}-61 / 2^{\prime \prime}$ VERTICAL RANGE


HD25
FIXED HEIGHT 1/4"


LO
1 1/4" - 2" VERTICAL RANGE


HD50
FIXED HEIGHT 1/2"

$2^{\text {L" }}-43 / 4^{\prime \prime}$ VERTICAL RANGE

$\mathrm{LC}+\mathrm{C} 4+\mathrm{C} 4$
9" - 12" VERTICAL RANGE

PRODUCT CHARACTERISTICS
-MAXIMUM DESIGN CAPACITY OF 750 LBS PER PEDESTAL, FACTOR OF SAFETY 3. -SCREW ADJUSTABILITY WHILE PEDESTALS ARE LOADED FOR FINAL. ADJUSTMENT. -IMPERVIOUS TO FREEZE-THAW, WATER, MOLD AND SOLVENT FREE CHEMICALS. -SCORED BASE ALLOWS SUPPORTS TO BE TRIMMED FOR TIGHT AREAS.
-WEIGHT BEARING SYSTEM DOES NOT PENETRATE ROOFING MEMBRANE OR SUBSTRATE. -LARGE FOOTPRINT SPREADS WEIGHT OVER ROOFING MEMBRANE AND SUBSTRATE.
-MAXIMUM CAVITY HEIGHT 12".
GENERAL NOTES: APPLY TO ALL OF THE ABOVE PRODUCTS

1. INSTALLATION MUST BE COMPLETED IN ACCORDANCE WITH BISON INNOVATIVE PRODUCTS SPECIFICATIONS.
2. DRAWINGS NOT TO SCALE.
3. CONTRACTOR'S NOTE: FOR PRODUCT AND COMPANY INFORMATION VISIT www.BisonIP.com


## SPECIFICATIONS



CANADA EFFICIENCIES EnerGuide (CSA P.4.1-15) - EnerGuide is a rating used in Camada to measure annual fireplace efliciency


For complete information on this model, please contact us at:

## heat clo

No one builds a better fire Wah heatnglo.com Phone: (888) 427-3973
E-mail: info a heatnglo.com
5 facebook.com/HeatandGlo
(1) (1) twitter:com/HeatandGlo

- youtube.com/HeatandGlo

LIMITED LIFETIME WARRANTY ${ }^{3}$
The strongest in the industry, Heat \& Glo provides a limited lifetime warranty on the most important aspects: furebox and heat exchanger.

3: For full warranty cietais see heatnglo.com
-rreplace glass and other surfaces get extremely HOT and can cause severe burns if touched. Do not remove the protective safety screen from the front of the glass. Keep a safe clistance away. To learn more visit wrwwheatnglo

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HNG-1134U-0520


COULTER ARCHITECTS, PLLC

October 26, 2021

Memo to: Melissa Jenck, CFM,


From: Coulter Architects, PLLC
RE: As a response to your letter of August 10, 2021, I have enclosed Drawing revisions to comply with the FEC Form from Bayside Surveying, and also removing all appliances from the lower level of the existing and new lower levels.

Melissa, Please replace the current drawings with the following revised drawings dated Oct. 11, 2021

## Enclosures:

Bayside Elevation Certificate, Signed by Dallas and myself as Dave's representative.
Architectural Drawings to be replaced:
Drawing A- 1.1 Upper left, shows the removal of the water Heater, which is being replaced by an on demand water heater on the upper floor.

Drawing A-1.2 shows the new on Demand water heater located in the store room next to the kitchen of the addition, and an on demand water heater in the closet of bedroom \#1 of the existing house.

Drawings A-2.1, A-2.2, and A-2.3 elevations, show the addition of the 10 smart vents discussed in the FEC form, and clarifies the location on both the existing and the new addition as being no more than 12" above grade.

I am sending these drawings both digitally and hard copy so they can be substituted in the existing drawing sets submitted previously.

Thanks for you help clarifying this.
Ronald E. Coulter, AIA, NCARB



Copy all pages of this Elevation Certificate and all attachments for (1) community official, (2) insurance agent/company, and (3) building owner.

| SECTION A - PROPERTY INFORMATION |  | FOR INSURANCE COMPANY USE |  |
| :---: | :---: | :---: | :---: |
| A1. Building Owner's Name David Coulter | Policy Number: |  |  |
| A2. Building Street Address (in Box No. <br> 35105 Rueppel Ave | Company NAIC Number: |  |  |
| City <br> Pacific City | ZIP Code |  |  |
| A3. Property Description (Lot and Block Numbers, Tax Parcel Number, Legal Description, etc.) Tax Lot 4700, 4701 and 48004 S 10W Section 30 BD |  |  |  |
| A4. Building Use (e.g., Residential, Non-Residential, Addition, Accessory, etc.) Residential |  |  |  |
| A5. Latitude/Longitude: Lat. 45-11-53.826 Long. -123-57-44.371 |  |  |  |
| A6. Attach at least 2 photographs of the building if the Certificate is being used to obtain flood insurance. |  |  |  |
| A7. Building Diagram Number |  |  |  |
| A8. For a building with a crawlspace or enclosure(s): |  |  |  |
| a) Square footage of crawlspace or enclosure(s) 0.00 sq ft |  |  |  |
| b) Number of permanent flood openings in the crawlspace or enclosure(s) within 1.0 foot above adjacent grade 0 |  |  |  |
| c) Total net area of flood openings in A8.b $\quad 0.00$ sq in |  |  |  |
| d) Engineered flood openings? $\square$ Yes $\triangle$ No |  |  |  |
| A9. For a building with an attached garage: |  |  |  |
| a) Square footage of attached garage 3204.00 sq ft |  |  |  |
| b) Number of permanent flood openings in the attached garage within 1.0 foot above adjacent grade 17 |  |  |  |
| c) Total net area of flood openings in A9.b 3400.00 sq in |  |  |  |
| d) Engineered flood openings? $\triangle$ Yes $\square$ No |  |  |  |

## SECTION B - FLOOD INSURANCE RATE MAP (FIRM) INFORMATION

| B1. NFIP Com Tillamook Cou | $\begin{aligned} & \text { ty Name \& } \\ & 10196 \end{aligned}$ | ommunity Number | B2. County Name TILLAMOOK |  | B3. State Oregon |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { B4. Map/Panel } \\ & \text { Number } \\ & 41057 \text { C0855 } \end{aligned}$ | B5. Suffix <br> F | $\begin{aligned} & \text { B6. FIRM Index } \\ & \text { Date } \\ & \text { 09-28-2018 } \end{aligned}$ | B7. FIRM Panel Effective/ Revised Date 09-28-2018 | B8. Flood Zone(s) <br> AE | B9. Base Flood Elevation(s) (Zone AO, use Base Flood Depth) 16.6 |

B10. Indicate the source of the Base Flood Elevation (BFE) data or base flood depth entered in Item B9:
$\square$ FIS Profile $\boxtimes$ FIRM $\square$ Community Determined $\square$ Other/Source: $\qquad$
B11. Indicate elevation datum used for BFE in Item B9:NGVD 1929NAVD 1988Other/Source: $\qquad$
B12. Is the building located in a Coastal Barrier Resources System (CBRS) area or Otherwise Protected Area (OPA)? $\square$ Yes $\boxtimes$ No Designation Date: $\qquad$CBRSOPA

## ELEVATION CERTIFICATE

OMB No. 1660-0008
Expiration Date: November 30, 2022

| IMPORTANT: In these spaces, copy the corresponding information from S | FOR INSURANCE COMPANY USE |
| :---: | :---: |
| Building Street Address (including Apt., Unit. Suite, and/or Bldg. No.) or P.O. R 35105 Rueppel Ave | Policy Number: |
| City State ZI <br> Pacific City Oregon 97 | Company NAIC Number |
| SECTION C - BUILDING ELEVATION INFORMATION (SURVEY REQUIRED) |  |
| C1. Building elevations are based on: $\square$ *A new Elevation Certificate will be required when construction of the buildin <br> C2. Elevations - Zones A1-A30, AE, AH, A (with BFE), VE, V1-V30, V (with BF Complete Items C2.a-h below according to the building diagram specified in Benchmark Utilized: GPS Vertical Datum: Indicate elevation datum used for the elevations in items a) through h) below. NGVD 1929 $\square$ Other/Source: $\qquad$ <br> Datum used for building elevations must be the same as that used for the B <br> a) Top of bottom floor (including basement, crawlspace, or enclosure floor) <br> b) Top of the next higher floor <br> c) Bottom of the lowest horizontal structural member (V Zones only) <br> d) Attached garage (top of slab) <br> e) Lowest elevation of machinery or equipment servicing the building (Describe type of equipment and location in Comments) <br> f) Lowest adjacent (finished) grade next to building (LAG) <br> g) Highest adjacent (finished) grade next to building (HAG) <br> h) Lowest adjacent grade at lowest elevation of deck or stairs, including structural support | ction* $\square$ Finished Construction <br> AE, AR/A1-A30, AR/AH, AR/AO. <br> Rico only, enter meters. <br> Check the measurement used. |

## SECTION D - SURVEYOR, ENGINEER, OR ARCHITECT CERTIFICATION

This certification is to be signed and sealed by a land surveyor, engineer, or architect authorized by law to certify elevation information. I certify that the information on this Certificate represents my best efforts to interpret the data available. I understand that any false statement may be punishable by fine or imprisonment under 18 U.S. Code. Section 1001.
Were latitude and longitude in Section A provided by a licensed land surveyor? $\boxtimes$ Yes $\square$ No $\square$ check here if attachments.



For Zones AO and A (without BFE), complete Items E1-E5. If the Certificate is intended to support a LOMA or LOMR-F request, complete Sections A, B, and C. For Items E1-E4, use natural grade, if available. Check the measurement used. In Puerto Rico only, enter meters.

E1. Provide elevation information for the following and check the appropriate boxes to show whether the elevation is above or below the highest adjacent grade (HAG) and the lowest adjacent grade (LAG).
a) Top of bottom floor (including basement, crawlspace, or enclosure) isfeetmetersabove orbelow the HAG.
b) Top of bottom floor (including basement, crawlspace, or enclosure) is $\qquad$feet $\qquad$ metersabove orbelow the LAG.

E2. For Building Diagrams 6-9 with permanent flood openings provided in Section A Items 8 and/or 9 (see pages 1-2 of Instructions), the next higher floor (elevation C2.b in the diagrams) of the building is $\qquad$feetmetersabove orbelow the HAG.

E3. Attached garage (top of slab) is $\qquad$feetmetersabove orbelow the HAG.

E4. Top of platform of machinery and/or equipment servicing the building is $\qquad$feetmetersabove orbelow the HAG.

E5. Zone AO only: If no flood depth number is available, is the top of the bottom floor elevated in accordance with the community's floodplain management ordinance?Yes $\square \mathrm{N}$ NoUnknown. The local official must certify this information in Section G.

## SECTION F - PROPERTY OWNER (OR OWNER'S REPRESENTATIVE) CERTIFICATION

The property owner or owner's authorized representative who completes Sections A, B, and E for Zone A (without a FEMA-issued or community-issued BFE) or Zone AO must sign here. The statements in Sections A, B, and E are correct to the best of my knowledge.


Check here if attachments.


E\&EVATION CERTIFICATE

| IMPORTANT: In these spaces, copy the corresponding information from Section A. | FOR INSURANCE COMPANY USE |  |
| :--- | :--- | :--- |
| Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No. | Policy Number: |  |
| 35105 Rueppel Ave |  |  |
| City | State | ZIP Code |
| Pacific City | Oregon | Company NAIC Number |

If using the Elevation Certificate to obtain NFIP flood insurance, affix at least 2 building photographs below according to the instructions for Item A6. Identify all photographs with date taken; "Front View" and "Rear View"; and, if required, "Right Side View" and "Left Side View." When applicable, photographs must show the foundation with representative examples of the flood openings or vents, as indicated in Section A8. If submitting more photographs than will fit on this page, use the Continuation Page.


ELEVATION CERTIFICATE
vivid ive. ivuu-uuvo

| IMPORTANT: In these spaces, copy the corresponding information from Section A. | FOR INSURANCE COMPANY USE |  |
| :--- | :--- | :--- |
| Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or P.O. Route and Box No. | Policy Number: |  |
| 35105 Rueppel Ave | State | ZIP Code |
| City | Oregon | Company NAIC Number |
| Pacific City |  |  |

If submitting more photographs than will fit on the preceding page, affix the additional photographs below. Identify all photographs with: date taken; "Front View" and "Rear View"; and, if required, "Right Side View" and "Left Side View." When applicable, photographs must show the foundation with representative examples of the flood openings or vents, as indicated in Section A8.



COULTER ARCHITECTS, PLLC

February 7, 2022
Hello Melissa;

## RE: Dave Coulter project

In response to your 2-3-22 email questions, I have for you the following:

## ELEVATOR:

I have enclosed the product cut sheets, which identifies how it is constructed, and he layout.

To reiterate, we discussed this at length back at the beginning, and I have addressed the issues as follows:

The motor is located at the top of the shaft above the car in the up position. This keeps it out of the way of the flooding, as well as the control panel being located above the flood level. (above the concrete lower portion of the ground floor walls.)

This unit is capable of being programmed to return to the upper level when not is use. ( at a set time delay.)

The shaft itself is also concrete to match the same configuration of the rest of the ground level walis.

We will also provide a submersible sump pump in the shaft pit to clear out any water that intrudes.


COULTER ARCHITECTS, PLLC

## THE EXISTING BUILDING ENTRY:

This has always been the entry to the building, and is an existing stairway with only some minor adjustments. The difference is, instead of opening a garage door for entry, we have a standard person door in a new exterior wall.

The floor is the original concrete garage floor, with new ceramic tile on top.
Any new framing could be treated lumber, which would provide some protection.

## VALUE:

We have discussed this previously and we gave you our estimated value number.

## Melissa Jenck

| From: | ronald coulter [ron.coulterarchitects@gmail.com](mailto:ron.coulterarchitects@gmail.com) |
| :--- | :--- |
| Sent: | Wednesday, September 29, 2021 9:07 AM |
| To: | Melissa Jenck |
| Subject: | EXTERNAL: Project value |

[NOTICE: This message originated outside of Tillamook County -- DO NOT CLICK on links or open attachments unless you are sure the content is safe.]

Good morning Melissa,

I know you are at a conference, but will send this along so you have it.

We are currently bidding the job with two contractors, one from Tillamook and one from Pacific City. We don't have the bids yet, so we don't even know what it will cost. With the volatility in the supply chain and the commodities, it's even difficult for the contractors to bid a job accurately without some provisions to adjust prices.

Second, based on the banking requirements, we can't get an appraisal until we have a signed contract with the contractor. This will be a while yet, until we have bids and can select a contractor.

We don't plan on getting two appraisals,

As a professional in this business, I can give you a number based on my experience. In Discussing This With Dave as well.....we would stipulate a price of $\$ 650,000$.

I have not received anything from Dallas yet.

Thanks,
Ron


## Statement

Pacific City Joint Water-Sanitary Authority
PO Box 520
Pacific City, OR 97135
(503) 965-6636
www.pcjwsa.com
DAVE AND PATTY COULTER 217 N GRANT ST
GOLDENDALE WA 98620-9513

## SPECIAL MESSAGE



## ACCOUNT INFORMATION

ACCOUNT:
002685-000
SERVICE ADDRESS:
SERVICE PERIOD:
BILLING DATE:
35465 RUEPPELL AVENUE 04/01/2021 to 04/30/2021 04/30/2021

DUE DATE: 05/17/2021

## BILLING DETAIL

## METER READING

|  | Previous | Previous | Current | Current |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Serial No | Read Date | Read | Read Date | Read | Cons |
| 2100022744 | $03 / 25 / 2021$ | 417 | $04 / 27 / 2021$ | 826 | 409 |

CURRENT CHARGES
Water 29.8
Sewer 35.06
Streetlights 0.45
Water Capital Improvement Charge 3
Sewer Capital Improvement Charge 5
WWTP Capital Improvement Charge 8.5
TOTAL CURRENT CHARGES 81.81
BILL SUMMARY
PREVIOUS BALANCE 81.89
PAYMENTS RECEIVED 81.89
ADJUSTMENTS 0.00
ADDITIONAL BILLING 0.00
CURRENT CHARGES 81.81
TOTAL AMOUNT DUE 81.81

PLEASE RETURN THIS PORTION ALONG WITH YOUR PAYMENT. PLEASE MAKE CHECK PAYABLE TO: PCJWSA


| ACCOUNT NUMBER | DUE DATE | TOTAL DUE |
| :---: | :---: | :---: |
| $002685-000$ | $05 / 17 / 2021$ | $\$ 81.81$ |
| Please Indicate <br> Amount Enclosed |  |  |


DAVE AND PATTY COULTER 217 N GRANT ST GOLDENDALE WA 98620-9513

י|
PCJWSA
PO BOX 520
PACIFIC CITY OR 97135-0520

Tillamook People's Utility District
PO Box 433
Tillamook, OR 97141-0433

| Billing Date | $04 / 08 / 2021$ |
| :--- | ---: |
| Account Number | 104503 |
| Payment Due | $05 / 03 / 2021$ |

Office Address:
1115 Pacific Ave, Tillamook, OR 97141
Hours: 7:00 AM-5:30 PM Monday-Thursday
Phone: (503) 842-2535 Fax: (503) 842-4161
Toll Free: (800) 422-2535 Web: www.tpud.org

| Billing Summary |  |  |
| :--- | :--- | :---: |
| Previous Balance |  |  |
| Payment Received 03/24/2021 | Thank you! | $\$ 128.95$ |
| Balance Forward | $\$ 128.95 \mathrm{CR}$ |  |
| Current Charges | $\$ 0.00$ |  |
| Total Balance |  | $\$ 147.66$ |

```
2132 1 AB 0.428
DAVID M COULTER
    5 2132
217 N GRANT ST
GOLDENDALE WA 98620-9513
```




[^3]RETURN BOTTOM PORTION WITH YOUR PAYMENT. PLEASE DO NOT FOLD, STAPLE, TAPE, OR PAPERCLIP.

| DAVID M COULTER <br> PATTIE FRITZ <br> 217 N GRANT <br> GOLDENDALE WA 98620-0000 | Amount Due | \$147.66 |
| :---: | :---: | :---: |
|  | Customer Assistance Donation |  |
|  | Amount Enclosed |  |
| Home: (360) 508-1050 <br> Work: None on File <br> Cell: None on File | Current Charges Due 05/03/2021 |  |
| Please notify us of any changes to your personal information below: | TILLAMOOK PEOPLE'S UTILITY DISTRICT PO BOX 433 <br> TILLAMOOK OR 97141-0433 <br>  | اווי\|IIIIIII |

## Connect With Us

Phone: 503.842.2535 Toll Free: 1.800.422.2535 - Office Hours: Monday - Thursday 7:00 a.m. - 5:30 p.m.
Address: P.O. Box 433 • 1115 Pacific Avenue, Tillamook, OR 97141
Emergency and after hours phone: 503.842.2122 or 1.800.842.2122


Website: www.tpud.org Email: service@tpud.org
SmartHub: An online application to pay your bill, view and monitor energy usage, report outages, and receive account notifications. Visit our website at www. tpud.org to learn more.
Nixle Alerts: Sign up for this alert system that allows us to send you important outage information via text message and/or email. Visit our website at www.tpud.org and click on the Nixle logo to sign up.

## Power Outages

If your power goes out: Check your fuses and breakers to ensure the problem is not within your electrical system. Report the outage immediately if you have determined the outage is on the Tillamook PUD system.
How to report a power outage:
By Phone: Call Tillamook PUD's 24-hour operation's center at 503.842.2122 or 1.800.842.2122 to report the location and circumstances of an outage. During large outages, the line may be busy due to the large volume of callers. Please continue to call until you get through or report the outage online.
Online: Use the SmartHub application to report an outage using your mobile device, tablet or personal computer.
For mobile and tablet users, login to your account via the SmartHub app. Once there, select the "Service Status" icon and then select the "Report My Power is Out" option.
When reporting through the Tillamook PUD website, www.tpud.org, click on the red text "Report An Outage" on the left side of the screen and log into your SmartHub account. Follow the prompts to report the outage.

## Help Your Neighbors in Need

The Customer Assistance Program (CAP) is Tillamook PUD's emergency assistance program to help spread warmth throughout our community. The long-standing CAP program is designed to assist limited-income families in crisis situations who need help paying their electric bills. Tillamook PUD matches the amount of every donation and it is placed into a fund where it provides twice the assistance. It's easy to make a one-time gift, sign-up for monthly recurring donations, or add extra to your monthly electric bill. Please help your neighbors in need through Tillamook PUD's Customer Assistance Program.

## Payment Options

## We accept your check, debit card, MasterCard and Visa

Online Payment: Visit our website at www.tpud.org and click on the SmartHub logo. All you'll need is your Tillamook PUD account number, which can be found on your electric bill, and a checking account number or a debit card, MasterCard or Visa.
Budget Billing: If you've lived in the same home for more than 12 months with Tillamook PUD, you may qualify for our Budget Billing plan. With Budget Billing, you make equal payments throughout the year, with a true-up annually.
Paperless Billing: This online resource is easy, convenient and saves resources by eliminating a paper bill each month. Go to SmartHub on our website and enter your email address and password. Click on the "My Profile" button, then click "Update My Printed Bill Settings", "Turn off/on Printed Bill."
Auto Pay: Automatically pay your monthly electric bill directly from your bank account or with a debit card, MasterCard or Visa. Combine Auto Pay with Budget and Paperless Billing to make your monthly payment predictable and simple. Please contact our front office staff to sign up for the Auto Pay option.
Office Counter, Drive-Through, Phone, or Drop Box: Drop by our office, use our drive-up window, or call 503.842 .2535 or 1.800.422.2535, Monday through Thursday, 7:00 a.m. - 5:30 p.m. A drop box is available at our drive through lane to make your payment outside these hours.

## Neopor® GPS Smart Insulation

## Neopor

- Innovation in Insulation

Neopor ${ }^{\circledR}$ GPS (Graphite Polystyrene) rigid insulation is today's energy-efficient and cost-effective insulation solution for architects, builders and contractors. The table shows data of Neopor ${ }^{\oplus}$ GPS F5300 Plus. $\qquad$ ave Coulter


1) Neopor ${ }^{\oplus}$ GPS meets and exceeds ASTM C578-13, "Standard Specification for Rigid, Cellular Polystyrene Thermal Insulation"; published by ASTM International, 100 Barr Harbor Drive, PO Box C700, West Conshohocken, PA 19428-2959.
2) $R$ means resistance to heat flow. The higher the $R$-value, the greater the insulating power. Ask your seller for the fact sheet on $R$-values.
3) The technical and physical metrics provided in this table are reference values for insulation products made of Neopor GPS. The values and properties may vary depending on how they are processed and produced. The R-value properties are based on 1-1/16 in thickness.

We create chemistry

## Material Ingredient Reporting for LEED v4, Option 1 Manufacturer Inventory

BASF Corporation certifies the following information for Neopor ${ }^{\otimes}$ F 5300 Plus - 30570155.
A complete content inventory for this product to $1,000 \mathrm{ppm}$ is provided based on the addenda to Option 1 of the Building product disclosure and optimization - material ingredients credit released by the U.S. Green Building Council on April 5, 2016. The information generated is based on the BASF Product Compliance Management Process which has been third party audited by GreenCircle Certified, LLC (GreenCircle). GreenCircle has verified that BASF's Product Compliance Management System assesses the hazards of all the ingredients that make up a product, including impurities. This assessment has verified all hazard classification, assessment and communication is conducted within the provisions of North American countries' regulatory requirements.

1. Publicly available ingredients are identified by name and Chemical Abstract Service Registration Number (CASRN)
2. Ingredients defined as trade secret or intellectual property have been withheld; however, the role, amount and hazards based on screening for the levels of ingredients presented are reported on this page per the requirements of the Globally Harmonized System of Classification and Labelling of Chemicals rev. 6 (2015).

## David Green

Applied Sustainability
BASF Corporation - Construction Chemicals

We create chemistry

| Publicly Available Ingredients |  |
| :---: | :---: |
| Substance Name | Substance CAS Number |
| polystyrene | $9003-53-6$ |
| Pentane | $109-66--0$ |
| Graphite | $7782-42-5$ |
| isopentane | $78-78-4$ |
| Sulfonium compounds, C11-14- <br> alkylbis(hydroxyethyl), 2- <br> hydroxyethyl sulfates (salts) | $78169-20-7$ |


| Proprietary Ingredients |  |  |
| :---: | :---: | :---: |
| Role for proprietary <br> substances | Ingredient Amount (\% by <br> weight) | Hazard Category |
| Polymer | $<5 \%$ | Below GHS reporting threshold |
| Additive | $<5 \%$ | Below GHS reporting threshold |
| Additive | $<5 \%$ | Below GHS reporting threshold |
| Additive | $<5 \%$ | Below GHS reporting threshold |
| Additive | $<5 \%$ | Below GHS reporting threshold |
| Additive | $<5 \%$ | Below GHS reporting threshold |
| Additive | $<5 \%$ | Below GHS reporting threshold |
| Residual Monomer | $<5 \%$ | Below GHS reporting threshold |
| Additive | $<5 \%$ | Below GHS reporting threshold |
| Additive | $<5 \%$ | Below GHS reporting threshold |

## Neopor ${ }^{\circledR}$ F 5300 Plus

## Application

Neopor*F 5300 Plus is an expandable polystyrene with increased graphite content which is used to manufacture silver-gray colored foams with a very low thermal conductivity.

The fire characteristics of these foams are in conformity with:

- DIN 4102-B1 (flame retardant)
- EN ISO 13501-1 class E

For additional information regarding fire fire behaviour, please contact your local BASF representative.

| Neopor F 5300 | For block molding, shape molding <br> (minimum wall thickness 30 mm ) and <br> Plus |
| :--- | :--- |
|  | loose fill applications. |

## Product description

Expandable polystyrene (EPS) with infrared reflecting additive. Contains uniformly distributed polymeric flame retardant.
Blowing agent (pentane) content approx. $5.3 \%$ by weight.

| Product | Bead size <br> class | Typical bead size |
| :--- | :--- | :--- |
| Neopor F 5300 <br> Plus | $0.9-1.4 \mathrm{~mm}$ | $0.8-1.5 \mathrm{~mm}$ <br> $(\geq 95 \%$ by weight) |

## Physical form

Neopor") F 5300 Plus is supplied in the form of a lentilshaped granulate.

## Storage

Neopor ${ }^{5}$ is usually supplied in cardboard containers (octabins). It can be stored in these unopened receptacles for three months before processing.

The octabins should not be exposed to weather conditions (rain, water, snow, frost, and sunlight) and must be protected from damage. They should always be stored in a cool place (below $20^{\circ} \mathrm{C}$ if possible) to minimize loss of blowing agent.

Once containers have been opened, their contents should be used as soon as possible. In the meantime the octabins should be kept tightly sealed.

It is not recommended to stack octabins more than one layer high. In case of double-stacking octabins under controlled conditions, a strong plywood board must be placed between the stacked containers.

Octabins covered with a plastic hood and/or shrinkwrapped should never be double stacked.

|  | Recom- <br> mended <br> intermediate <br> aging period | Achievable <br> bulk density <br> by single step <br> pre-expansion |  |
| :--- | :--- | :--- | :--- |
| Product | density-range |  |  |
| Neopor $\mathrm{F}^{2}$ <br> 5300 Plus | $12^{*}-20 \mathrm{~kg} / \mathrm{m}^{3}$ | $10-48 \mathrm{~h}$ | $17 \mathrm{~kg} / \mathrm{m}^{3}$ |

[^4]
## Processing

The raw material must not be mixed with other raw materials in order to comply with the requirements of fire test certificates.

Neopor ${ }^{5}$ is processed into foam in 3 steps.

## - Preexpansion

Neopor" F 5300 Plus can be preexpanded to the above-mentioned densities without any problems using discontinuous, state-of-the-art preexpanders. Lower densities can be achieved by double step preexpansion.

## - Intermediate aging

The intermediate aging time should be selected depending on the bulk density, the ambient temperature and the intended application. It is usually between 10 and 48 hours.

## - Molding

Neopor ${ }^{\text {® }}$ F 5300 Plus can be molded in commercially available block- and shapemolding machines. Due to the slightly lenticular shape of the particles, adjustments to the filling systems of the shapemolding machines may be necessary.

If recycling material is to be added, it must be ensured that the density of the recycling material is as closely as possible to the preexpansion density in order to avoid separation effects in the molds. Moreover it is recommended to work up the recycling material in a dedusting system before use.

For further information regarding processing, please contact your local BASF contact person.

Further information about the properties and uses of Neopor ${ }^{5}$ is given at www.neopor.de

## Packaging

Sheets and molded parts made of Neopor must not be packed in transparent films. The use of an opaque/white or dyed film is strongly recommended.

## Safety precautions

It should be noted, that during the processing and storage of Neopor. as well as of foams produced from it, explosive blowing agent/air mixtures may be formed by diffusing blowing agent (pentane, LEL 1.3 vol\%).

Therefore, adequate ventilation must be provided at all times. All conceivable ignition sources (open flames, welding sparks, electrical sparks etc.) must be kept away and electrostatic charging must be avoided. Smoking must be strictly prohibited!

It is forbidden to transport Neopore raw material or Neopor foam in unventilated or closed vehicles. Further information is given in the respective safety data sheet.

## Industrial hygiene

Pentane escapes during storage and processing of Neopors. The workplace should therefore be well ventilated. Especially when hot-wire cutting the foams, it is important to ensure that the vapours produced are extracted, as they contain small amounts of styrene in addition to pentane.

The regionally applicable workplace concentration limits for styrene and pentane must be observed.

## Foodstuffs legislation

Foams made of Neopor shall not be used in direct contact with food.

## Note

The data contained in this publication are based on our current knowledge and experience. In view of the many factors that may affect processing and application of our product, these data do not relieve processors from carrying out their own investigations and tests; neither do these data imply any guarantee of certain properties, nor the suitability of the product for a specific purpose. Any descriptions, drawings, photographs, data, proportions, weights etc. given herein may change without prior information and do not constitute the agreed contractual quality of the product. It is the responsibility of the recipient of our products to ensure that any proprietary rights and existing laws and legislation are observed.









## 35465 Rueppell Avenue PACIFIC CITY, OR

## Hydraulics Analysis Report


prepared for
David Coulter
prepared by
Jake Hofeld, P.E.


WATERWAYS<br>CONSULTING, INC.

March 30, 2021

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Figure 2: Hydraulic Analysis Overview Map of Proposed Project
Figure 3: Existing Conditions Site Plan
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Figure 5: Proposed Conditions Elevation Section

## List of Attachments

Attachment A - HEC-RAS Model Output Files

## INTRODUCTION

Waterways Consulting Inc. (Waterways) has been retained by David Coulter to evaluate the hydraulic effects on the Nestucca River during a 100-year base flood discharge from a proposed residential structure. The proposed residential structure is located on the east (left) bank floodplain of the Nestucca River at 35465 Rueppell Avenue in Pacific City, Oregon. The existing site is currently a residential singlefamily home with a grassy backyard adjacent to the Pacific City State Airport.

The proposed development on the parcel will add a two-story structure with a second story living space and a ground floor garage with an abutting open carport. A gravel driveway will be graded to provide access to the garage and carport in addition to a retaining wall located at the east edge of the carport. The entire property being developed will occur within the FEMA designated floodway, effective September 28, 2018 (Figure 1).

The following report has been prepared to support floodplain development permitting with Tillamook County for the proposed project and presents our hydraulic analysis of existing and proposed conditions for the 100-year flood event along the Nestucca River within the vicinity of the proposed residential structure. This report is based on the guidance outlined in Section 3.510(9)(a) of the Tillamook County Land Use Ordinance which requires, "...certification is provided by a professional registered civil engineer demonstrating through hydrologic and hydraulic analysis performed in accordance with standard engineering practice that such encroachment shall not result in any increase in flood levels during the occurrence of the based flood discharge."

## HYDRAULIC MODELING METHODOLOGY

The Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) has mapped Nestucca River at the project area as a Special Flood Hazard Area (SFHA) within the regulatory floodway Zone AE (Figure 1). Tillamook County provided Waterways with a hydraulic model of the Nestucca River covering the project area for a Letter of Map Revision (LOMR), effective September 24, 2015 (Case. Number 14-10-1727P). The LOMR and corresponding hydraulic model conducted in the United States Army Corps of Engineers (USACE) Hydraulic Engineering Center River Analysis Software (HEC-RAS) by West Consultants updated the previous modeling and FIRM Panels dated August 1, 1978. All elevations are referenced to a NAVD 88 vertical datum. This model was used as the basis for all hydraulic modeling.

Waterways updated the hydraulic analysis using HEC-RAS, version 5.0.7. A one-dimensional hydraulic model was completed to characterize the existing and proposed conditions at the project site during the 100-year recurrence interval peak flow at the Nestucca River. Additional cross sections were added to the provided model in the vicinity of the project area. The two modeling scenarios include the Existing Conditions Model ("Ex. Cond." is the Plan identifier in the model) and the Proposed Conditions Model ("Prop. Cond." is the Plan identifier in the model). Figure 2 shows the proposed project location, cross section locations used in the hydraulic analysis, and the effective FEMA floodplain and floodway boundaries (FEMA 2018).

## Existing Conditions Model

Additional cross sections added to the LOMR model were sampled from a terrain surface derived from LiDAR data from the Department of Geology and Mineral Industries (DOGAMI) North Coast collected by Watershed Sciences Inc. in 2009. LiDAR was updated and overlain with existing topographic survey data for the project parcel. The existing topographic survey was provided by the Domus Design Build, dated January 19, 2021 (Figure 3). Bathymetry for the additional cross sections were interpolated from upstream and downstream cross sections of the LOMR model.

The downstream model boundary extends approximately 1.1 miles downstream of the project area and the upstream model boundary extends approximately 2.7 miles upstream of the project area (Figure 2). The bridge crossing geometry at Ferry Street and at Pacific Avenue downstream of the project area were included in the model from drawings provided by Oregon Department of Transportation (ODOT) and Tillamook County. Hydraulic roughness values for the additional cross sections were based on values published in the provided model. Hydraulic roughness values, known as Manning's Roughness, for the additional cross sections are outlined in Table 1.

Table 1. Manning's Roughness for Different Land Use Types

| Land Use Type | Manning's ' $n$ ' |
| :--- | :---: |
| Channel | 0.03 |
| Gravel Driveway | 0.03 |
| Open Pervious Areas (grassed) | $0.04-0.05$ |
| Residential Area | 0.08 |
| Open Pervious Areas (trees) | 0.10 |

## Proposed Conditions Model

The proposed conditions model included the additional cross sections created in the existing conditions model. The existing conditions terrain was updated with the approximate proposed garage structure first floor footprint of 46 feet by 37 feet provided by design drawings supplied from the client (Figure 4). The proposed residential structure was modeled as a blocked obstruction at cross sections located at the upstream and downstream sides of the proposed structure. The location of the proposed structure is approximate due to the surveyed property boundaries being in an arbitrary horizontal datum but is considered accurate enough for the purposes of this analysis. The existing terrain was also updated with the grading of the gravel driveway provided by design drawings supplied from the client (Figures 4 and 5). The proposed open carport finished ground elevation was modeled as a blocked obstruction up to the finished ground elevation of 13.0 feet on the upstream and downstream sides of the proposed structure. The proposed gravel driveway slopes down from the finished floor of the garage and finished ground at the carport to an elevation of 12.67 feet which adds additional gravel fill to cross section located at the downstream side of the proposed structure and existing house. Structural posts supporting the raised roof deck over the carport were not included in the model because these are
assumed to have negligible effect on the river hydraulics (i.e. the river can flow unimpeded through these areas).

## Boundary Conditions

The downstream boundary condition used in the two models was set to a known water surface elevation of 14.15 feet (NAVD 88) per the provided model. The downstream boundary condition is located downstream of FEMA Cross Section A near where Nestucca River meets the Nestucca Bay.

## Peak Flow Hydrology

According to the FEMA FIS report and the provided model, the 100-year peak flow event for this portion of the Nestucca River is 49,700 cubic feet per second (cfs). Therefore, 49,700 cfs was assumed for the 100-year peak flow (i.e. base flood discharge) in all models.

## RESULTS

Results of the hydraulic modeling are presented in Attachment A. These results show that the proposed building will not result in a rise in water surface elevations anywhere in the model. No change between the Existing Conditions Model and Proposed Conditions Model can likely be attributed to the relatively small building footprints and minor grade change as compared to a much larger/wider floodplain area.

## CONCLUSIONS

The results of this hydraulic analysis indicated no rise in the 100-year water surface elevations for the Proposed Conditions Model when compared to the Existing Conditions Model. Based on this, the proposed project satisfies the requirement of Section 3.510(9)(a) of the Tillamook County Land Use Ordinance.


## REFERENCES

Federal Emergency Management Agency. 2018. Flood Insurance Rate Maps (FIRMs) for Tillamook County (panel 0855), Oregon and Incorporated Areas. September 28, 2018.

Federal Emergency Management Agency. 2018. Flood Insurance Study (FIS) for Tillamook County, Oregon and Incorporated Areas. September 8, 2018.

Domus Design Build. Site Plan Dave and Pattie Coulter 35465 Rueppell Ave. Pacific City, Oregon. January 19, 2021.
U.S. Army Corps of Engineers. Hydrologic Engineering Center. Computer Program HEC-RAS Version 5.0.7 Davis, California. March 2019.
U.S. Army Corps of Engineers. Hydrologic Engineering Center. Hydraulic Reference Manual. Version 5.0 Davis, California. February 2016.

Watershed Sciences. LiDAR Remote Sensing Data Collection Oregon North Coast. Prepared for Department of Geology and Mineral Industries (DOGAMI). December 21, 2009.

West Consultants. Hydraulic Engineering Center River Analysis Software (HEC-RAS) Model of the Nestucca River. 2014.

## Figures



FIGURE 1: FEMA FIRM PANEL





## Attachment A

## HEC-RAS Output Files

| Reach | River Sta | Profile | Plan | Q Total | Min ChEl | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude \# Chl |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | (cfs) | (fi) | (ft) | (fi) | (fi) | (f/ft) | (ft/s) | (sq fi) | (ft) |  |
| Lower | 22553.94 | 100-YR | Ex. Cond. | 49700.00 | -5.99 | 20.50 | 12.22 | 20.55 | 0.000090 | 3.06 | 32247.60 | 3644.65 | 0.11 |
| Lower | 22553.94 | 100-YR | Prop. Cond. | 49700.00 | -5.99 | 20,50 | 12.22 | 20.55 | 0.000090 | 3.06 | 32247.83 | 3644.66 | 0.11 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 21008.6 | 100-YR | Ex. Cond. | 49700.00 | -8.92 | 20.09 |  | 20.31 | 0.000259 | 5.18 | 17865.91 | 1743.77 | 0.20 |
| Lower | 21008.6 | 100-YR | Prop. Cond. | 49700.00 | -8.92 | 20.09 |  | 20.31 | 0.000259 | 5.18 | 17866.07 | 1743.77 | 0.20 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 20157.05 | 100-YR | Ex. Cond. | 49700.00 | -9.15 | 19.94 | 12.36 | 20.10 | 0.000212 | 4.43 | 20015.00 | 2302.29 | 0.17 |
| Lower | 20157.05 | 100-YR | Prop. Cond. | 49700.00 | -9.15 | 19.94 | 12.36 | 20.10 | 0.000212 | 4.43 | 20015.19 | 2302.29 | 0.17 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 19079.89 | 100-YR | Ex. Cond. | 49700.00 | -11.85 | 19.70 |  | 19.89 | 0.000228 | 5.02 | 20295.96 | 1888.75 | 0.18 |
| Lower | 19079.89 | 100-YR | Prop. Cond. | 49700.00 | -11.85 | 19.70 |  | 19.89 | 0.000228 | 5.02 | 20296.16 | 1888.75 | 0.18 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 18019.8 | 100-YR | Ex. Cond. | 49700.00 | -7.69 | 19.54 | 11.35 | 19.68 | 0.000186 | 4.31 | 22190.83 | 2668.25 | 0.16 |
| Lower | 18019.8 | 100-YR | Prop. Cond. | 49700.00 | -7.69 | 19.54 | 11.35 | 19.68 | 0.000186 | 4.31 | 22191.05 | 2668.26 | 0.16 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 17875.97 | 100-YR | Ex. Cond. | 49700.00 | -7.60 | 19.52 | 11.05 | 19.65 | 0.000168 | 4.13 | 23065.31 | 2677.05 | 0.16 |
| Lower | 17875.97 | 100-YR | Prop. Cond. | 49700.00 | -7.60 | 19.52 | 11.05 | 19.65 | 0.000168 | 4.13 | 23065.55 | 2677.05 | 0.16 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 17653.2 | 100-YR | Ex. Cond. | 49700.00 | -4.67 | 19.54 | 11.28 | 19.61 | 0.000095 | 3.21 | 29282.63 | 3181.65 | 0.12 |
| Lower | 17653.2 | 100-YR | Prop. Cond. | 49700.00 | -4.67 | 19.54 | 11.28 | 19.61 | 0.000095 | 3.21 | 29282.93 | 3181.65 | 0.12 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 15949.74 | 100-YR | Ex. Cond. | 49700.00 | -7.67 | 19.49 | 9.86 | 19.52 | 0.000032 | 1.90 | 46748.95 | 4377.64 | 0.07 |
| Lower | 15949.74 | 100-YR | Prop. Cond. | 49700.00 | -7.67 | 19.49 | 9.86 | 19.52 | 0.000032 | 1.90 | 46749.38 | 4377.65 | 0.07 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 14728.64 | 100-YR | Ex. Cond. | 49700.00 | -9.90 | 19.44 | 10.23 | 19.48 | 0.000043 | 2.46 | 37331.63 | 3855.78 | 0.09 |
| Lower | 14728.64 | 100-YR | Prop. Cond. | 49700.00 | -9.90 | 19.44 | 10.23 | 19.48 | 0.000043 | 2.46 | 37332.01 | 3855.78 | 0.09 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 14621.23 |  |  | Bridge |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 14544.91 | 100-YR | Ex. Cond. | 49700.00 | -8.62 | 19.42 | 10.32 | 19.46 | 0.000045 | 2.54 | 36915.93 | 3871.12 | 0.10 |
| Lower | 14544.91 | 100-YR | Prop. Cond. | 49700.00 | -8.62 | 19.42 | 10.32 | 19.46 | 0.000045 | 2.54 | 36916.31 | 3871.12 | 0.10 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 13541.26 | 100-YR | Ex. Cond. | 49700.00 | -7.81 | 19.38 | 10.21 | 19.42 | 0.000052 | 2.50 | 32796.95 | 3280.39 | 0.10 |
| Lower | 13541.26 | 100-YR | Prop. Cond. | 49700.00 | -7.81 | 19.38 | 10.21 | 19.42 | 0.000052 | 2.50 | 32797.25 | 3280.39 | 0.10 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 12396 | 100-YR | Ex. Cond. | 49700.00 | -3.59 | 18.51 |  | 19.22 | 0.000462 | 7.06 | 9099.18 | 2050.30 | 0.30 |
| Lower | 12396 | 100-YR | Prop. Cond. | 49700.00 | -3.59 | 18.51 |  | 19.22 | 0.000462 | 7.06 | 9099.27 | 2050.30 | 0.30 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 11367.2 | 100-YR | Ex. Cond. | 49700.00 | -3.05 | 17.74 | 9.51 | 18.66 | 0.000619 | 7.83 | 7539.82 | 2019.55 | 0.34 |
| Lower | 11367.2 | 100-YR | Prop. Cond. | 49700.00 | -3.05 | 17.74 | 9.51 | 18.66 | 0.000619 | 7.83 | 7539.93 | 2019.58 | 0.34 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 10048.77 | 100-YR | Ex. Cond. | 49700.00 | -3.49 | 16.99 | 9.18 | 17.82 | 0.000617 | 7.52 | 8689.80 | 2063.64 | 0.34 |
| Lower | 10048.77 | 100-YR | Prop. Cond. | 49700.00 | -3.49 | 16.99 | 9.18 | 17.82 | 0.000617 | 7.52 | 8690.02 | 2063.67 | 0.34 |


| Reach | River Sta | Profile | Plan | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude \# Chl |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | (cfs) | (ft) | (f) | (fi) | (f) | (flft) | (fl/s) | (sq fi) | (f) |  |
| Lower | 9942.323 |  |  | Bridge |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 9904.361 | 100-YR | Ex. Cond. | 49700.00 | -8.44 | 16.84 | 8.05 | 17.52 | 0.000540 | 6.93 | 10040.74 | 2094.21 | 0.31 |
| Lower | 9904.361 | 100-YR | Prop. Cond. | 49700.00 | -8.44 | 16.84 | 8.05 | 17.52 | 0.000540 | 6.93 | 10040.98 | 2094.21 | 0.31 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 8988.11 | 100-YR | Ex. Cond. | 49700.00 | -4.80 | 16.62 | 8.14 | 16.98 | 0.000328 | 5.35 | 12974.76 | 1987.89 | 0.24 |
| Lower | 8988.11 | 100-YR | Prop. Cond. | 49700.00 | -4.80 | 16.62 | 8.14 | 16.98 | 0.000328 | 5.35 | 12975.12 | 1987.91 | 0.24 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 8192.259 | 100-YR | Ex. Cond. | 49700.00 | -18.19 | 16.37 | 6.30 | 16.73 | 0.000306 | 5.46 | 12950.26 | 2042.12 | 0.23 |
| Lower | 8192.259 | 100-YR | Prop. Cond. | 49700.00 | -18.19 | 16.37 | 6.30 | 16.73 | 0.000306 | 5.46 | 12950.67 | 2042.12 | 0.23 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 8165 | 100-YR | Ex. Cond. | 49700.00 | -17.33 | 16.36 | 6.23 | 16.72 | 0.000285 | 5.38 | 13042.24 | 1970.46 | 0.23 |
| Lower | 8165 | 100-YR | Prop. Cond. | 49700.00 | -17.33 | 16.36 | 6.23 | 16.73 | 0.000290 | 5.42 | 12717.24 | 1924.26 | 0.23 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 8131 | 100-YR | Ex. Cond. | 49700.00 | -16.25 | 16.34 | 6.32 | 16.71 | 0.000297 | 5.49 | 12737.63 | 1923.02 | 0.23 |
| Lower | 8131 | 100-YR | Prop. Cond. | 49700.00 | -16.25 | 16.33 | 6.32 | 16.72 | 0.000303 | 5.54 | 12447.08 | 1876.78 | 0.23 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 8092 | 100-YR | Ex. Cond. | 49700.00 | -15.01 | 16.34 | 6.28 | 16.70 | 0.000269 | 5.27 | 12608.40 | 1838.87 | 0.23 |
| Lower | 8092 | 100-YR | Prop. Cond. | 49700.00 | -15.01 | 16.34 | 6.28 | 16.69 | 0.000261 | 5.19 | 12569.58 | 1839.59 | 0.22 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 8061 | 100-YR | Ex. Cond. | 49700.00 | -14.02 | 16.34 | 6.35 | 16.68 | 0.000278 | 5.15 | 12768.88 | 1825.31 | 0.22 |
| Lower | 8061 | 100-YR | Prop. Cond. | 49700.00 | -14.02 | 16.34 | 6.35 | 16,68 | 0.000278 | 5.15 | 12768.88 | 1825.31 | 0.22 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 8031 | 100-YR | Ex. Cond. | 49700.00 | -14.02 | 16.35 |  | 16.67 | 0.000266 | 5.01 | 13841.53 | 1832.03 | 0.22 |
|  | 8031 | 100-YR | Prop. Cond. | 49700.00 | -14.02 | 16.35 |  | 16.67 | 0.000266 | 5.01 | 13841.53 | 1832.03 | 0.22 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower <br> Lower | 7839.108 | 100-YR | Ex. Cond. | 49700.00 | -6.96 | 16.25 | 6.76 | 16.61 | 0.000310 | 5.16 | 12464.76 | 1879.15 | 0.23 |
|  | 7839.108 | 100-YR | Prop. Cond. | 49700.00 | -6.96 | 16.25 | 6.76 | 16.61 | 0.000310 | 5.16 | 12464.76 | 1879.15 | 0.23 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 6628.945 | 100-YR | Ex. Cond. | 49700.00 | -1.36 | 16.04 | 6.84 | 16.27 | 0.000208 | 3.91 | 14212.35 | 3171.30 | 0.19 |
| Lower | 6628.945 | 100-YR | Prop. Cond. | 49700.00 | -1.36 | 16.04 | 6.84 | 16.27 | 0.000208 | 3.91 | 14212.35 | 3171.30 | 0.19 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower | 4746.314 | 100-YR | Ex. Cond. | 49700.00 | -11.72 | 14.76 | 7.45 | 15.56 | 0.000672 | 7.30 | 7417.23 | 2442.34 | 0.34 |
| Lower | 4746.314 | 100-YR | Prop. Cond. | 49700.00 | -11.72 | 14.76 | 7.45 | 15.56 | 0.000672 | 7.30 | 7417.23 | 2442.34 | 0.34 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower <br> Lower | 3370.732 | 100-YR | Ex. Cond. | 49700.00 | -3.40 | 14.28 | 6.63 | 14.73 | 0.000430 | 5.53 | 9803.55 | 3594.57 | 0.27 |
|  | 3370.732 | 100-YR | Prop. Cond. | 49700.00 | -3.40 | 14.28 | 6.63 | 14.73 | 0.000430 | 5.53 | 9803.55 | 3594.57 | 0.27 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lower <br> Lower | 2099.855 | 100-YR | Ex. Cond. | 49700.00 | -3.90 | 14.15 | 5.85 | 14.31 | 0.000175 | 3.42 | 17693.71 | 5262.50 | 0.17 |
|  | 2099.855 | 100-YR | Prop. Cond. | 49700.00 | -3.90 | 14.15 | 5.85 | 14.31 | 0.000175 | 3.42 | 17693.71 | 5262.50 | 0.17 |



$$
R S=21008.6
$$










$R S=14621.23 B R$











$$
\text { RS }=8192.259
$$










$$
R S=4746.314
$$






## Melissa Jenck

| From: | Crowley, Josha [Josha.Crowley@atkinsglobal.com](mailto:Josha.Crowley@atkinsglobal.com) |
| :--- | :--- |
| Sent: | Monday, April 26, 2021 8:51 AM |
| To: | Melissa Jenck |
| Subject: | RE: EXTERNAL: Fwd: David Coulter |

Melissa - this looks good to me. No comments.

Josha Crowley, PE, PMP, CFM, D.WRE
RSC Lead | STARR II - Region X Service Center
Phone: (425) 329-3679
Cell: (206) 499-2440

From: Melissa Jenck [mjenck@co.tillamook.or.us](mailto:mjenck@co.tillamook.or.us)
Sent: Monday, April 19, 2021 3:32 PM
To: Crowley, Josha [Josha.Crowley@atkinsglobal.com](mailto:Josha.Crowley@atkinsglobal.com)
Subject: FW: EXTERNAL: Fwd: David Coulter

Good afternoon Josha,

Another day, another model (-) I hope I'm not keeping you too busy! I've got another no-rise for a property in Nestucca. Can you please review for compliance?

Thank you much!

Melissa Jenck | CFM, Land Use Planner II
Phone (503) 842-3408 x3301
(she/her)

The Department is excited to announce that we are OPEN to the public by appointment. To review the list of services provided and to schedule an appointment with us, please visit https://www.co.tillamook.or.us/gov/ComDev/ to access the appointment scheduler portal.

From: ronald coulter [ron.coulterarchitects@gmail.com](mailto:ron.coulterarchitects@gmail.com)
Sent: Monday, April 19, 2021 12:31 PM
To: Melissa Jenck [mjenck@co.tillamook.or.us](mailto:mjenck@co.tillamook.or.us)
Subject: EXTERNAL: Fwd: David Coulter
[NOTICE: This message originated outside of Tillamook County -- DO NOT CLICK on links or open attachments unless you are sure the content is safe.]

I'm forwarding Jake's final report.....this has both the PDF and the computer model.
Per our discussion this morning.
thanks Melissa

From: Jake Hofeld [jakeh@watways.com](mailto:jakeh@watways.com)
Date: Tue, Mar 30, 2021 at 1:27 PM
Subject: RE: David Coulter
To: ronald coulter [ron.coulterarchitects@gmail.com](mailto:ron.coulterarchitects@gmail.com)

Hi Ron,

Attached is our report and the associated hydraulic model for you to send to the County. Please let me know if you have any questions.

Thanks,

Jake D. Hofeld PE/CWRE

Senior Engineer

Waterways Consulting, Inc.

503-528-4816
www.watways.com

From: Jake Hofeld
Sent: Monday, March 29, 2021 1:31 PM
To: ronald coulter [ron.coulterarchitects@gmail.com](mailto:ron.coulterarchitects@gmail.com)
Subject: RE: David Coulter

Hi Ron,

The next step will be for me to finalize the hydraulic analysis model and report for you to send to the County with your permit application. I expect to have this over to you by tomorrow.

Thanks,
-Jake

From: ronald coulter [ron.coulterarchitects@gmail.com](mailto:ron.coulterarchitects@gmail.com)
Sent: Monday, March 29, 2021 12:56 PM
To: Jake Hofeld [jakeh@watways.com](mailto:jakeh@watways.com)
Subject: David Coulter

What's the next step......do I review, then you send to the county?

Hope you had a great vacation on the coast.

Ron

[^5]
[^0]:    Sarah Absher, CFM, Director
    Enc. Applicable Ordinance Criteria, Maps ,

[^1]:    105 N. Emerson Street, Suite 201 . Chelan, Washington
    Mail: P.O. Box 2323. Lake Chelan, WA 98816
    Office: 509.630 .5518

[^2]:    105 N . Emerson Street. Suite 201. Chelan. Washington
    Mail: P.O. Box 2323. Lake Chelan. WA 98816
    Office: 509.630 .5518

[^3]:    Message from Tillamook PUD
    Click on the Nixle logo on our home page at www.tpud.org to sign up to receive important outage alerts from Tillamook PUD via email
    or text messages.

[^4]:    'by double pass expansion

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